

Alternate way - without calculating I_S

For $V_{BE} = 0.7V$

$$\frac{i_C}{10mA} = e^{\frac{0.7 - 0.76}{0.025}}$$

$$\therefore i_C = \underline{0.907mA}$$

For $i_C = 10\mu A$

$$\frac{10 \times 10^{-6}}{10 \times 10^{-3}} = e^{\frac{V_{BE} - 0.76}{0.025}}$$

$$V_{BE} = \underline{0.587V}$$

5.9

$$\beta = \frac{\alpha}{1-\alpha}, \text{ for } \alpha \rightarrow \alpha + \Delta\alpha$$

$$\beta \rightarrow \beta + \Delta\beta$$

$$\beta + \Delta\beta = \frac{\alpha + \Delta\alpha}{1 - \alpha - \Delta\alpha} \text{ solve for } \Delta\beta$$

$$\Delta\beta = \frac{\alpha + \Delta\alpha}{1 - \alpha - \Delta\alpha} - \frac{\alpha}{1 - \alpha}$$

$$= \frac{\alpha}{1 - \alpha} \cdot \frac{1 + \frac{\Delta\alpha/\alpha}{1 - \frac{\Delta\alpha}{1 - \alpha}}} - \frac{\alpha}{1 - \alpha}$$

$$= \beta \times \frac{\frac{\Delta\alpha/\alpha}{1 - \frac{\Delta\alpha}{1 - \alpha}}}{1 - \frac{\Delta\alpha}{1 - \alpha}}$$

Thus,

$$\frac{\Delta\beta}{\beta} = \frac{\Delta\alpha}{\alpha} \cdot \frac{1 + \frac{\alpha}{1 - \alpha}}{1 - \frac{\Delta\alpha}{1 - \alpha}}$$

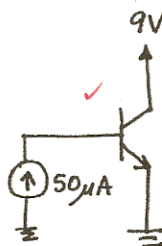
$$= \frac{\Delta\alpha}{\alpha} \frac{1 - \alpha + \alpha}{1 - \alpha - \Delta\alpha}$$

$$= \frac{\Delta\alpha}{\alpha} \frac{1}{1 - \alpha - \Delta\alpha}$$

for small $\Delta\alpha$, $\frac{1}{1 - \alpha - \Delta\alpha} \approx \beta$

$$\therefore \frac{\Delta\beta}{\beta} \approx \left(\frac{\Delta\alpha}{\alpha} \right) \beta \quad \text{Q.E.D.}$$

5.10



$$\beta = 60 \text{ to } 300 \checkmark$$

$$I_C = \beta I_B \text{ ranges from}$$

$$= 60 \times 50\mu A \text{ to } 300 \times 50\mu A$$

$$= \underline{3mA \text{ to } 15mA} \checkmark$$

$$I_E = I_C + I_B \text{ ranges from}$$

$$= \underline{3.05mA \text{ to } 15.05mA} \checkmark$$

$$\text{Max Power} = 9 \times I_{Cmax} = 9 \times 15$$

$$= \underline{135mW} \checkmark$$

5.11

$$i_C = I_S e^{V_{BE}/V_T}$$

$$10 \times 10^{-3} = I_S e^{0.7/0.025}$$

$$\Rightarrow I_S = 6.91 \times 10^{-15} A$$

$$\alpha = \frac{i_C}{i_C + i_B} = \frac{10}{10 + 0.1} = 0.990$$

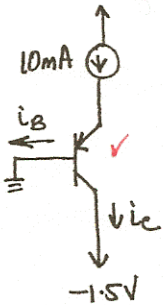
$$\beta = \frac{i_C}{i_B} = \frac{10}{0.1} = 100$$

$$\frac{I_S}{\alpha} = 6.98 \times 10^{-15} A$$

$$\frac{I_S}{\beta} = 6.91 \times 10^{-17} A$$

for $i_c = 10 \text{ mA}$ $V_{EB} = 0.685 \text{ V}$
 $i_c = 5 \text{ A}$ $V_{EB} = 0.840 \text{ V}$

5.18



$\beta = 10$

$i_c = \alpha i_E = \frac{10}{11} \times 10 = 9.09 \text{ mA} \checkmark$

$i_B = i_E - i_c = 0.91 \text{ mA} \checkmark$

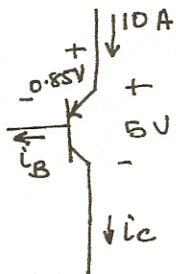
$i_c = I_s e^{V_{EB}/V_T}$
 $9.09 \times 10^{-3} = 10^{-16} e^{V_{EB}/0.025}$

$V_E = V_{EB} = 0.803 \text{ V} \checkmark$

For $\beta = 1000$

$i_c = \frac{\beta}{\beta+1} i_E = \frac{1000}{1001} \times 10 = 9.99 \text{ mA} \checkmark$

5.19



for $\beta = 15$

$i_E = (\beta+1) i_B$

$10 = (\beta+1) i_B$

$i_B = \frac{10}{16} = 0.625 \text{ A} \checkmark$

Calculating I_{S1}

$i_c = \frac{\beta}{\beta+1} i_E = I_{S1} e^{V_{EB}/V_T}$

$\frac{15}{16} \times 10 = I_{S1} e^{0.85/0.025}$

$I_{S1} = 1.608 \times 10^{-14} \text{ A}$

Compare this to

$I_{S2} = i_c e^{-V_{EB}/V_T}$
 $= 10^{-3} e^{-0.7/0.025}$
 $= 6.914 \times 10^{-16}$

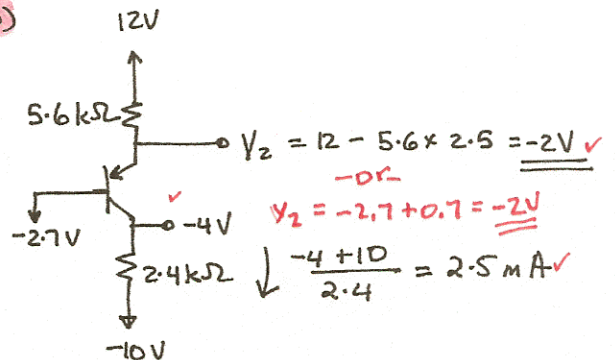
$\therefore I_S \propto \text{Area}$

$\frac{\text{Area 1}}{\text{Area 2}} = \frac{I_{S1}}{I_{S2}} = \frac{1.608 \times 10^{-14}}{6.914 \times 10^{-16}}$
 $= 23.3 \text{ times larger}$

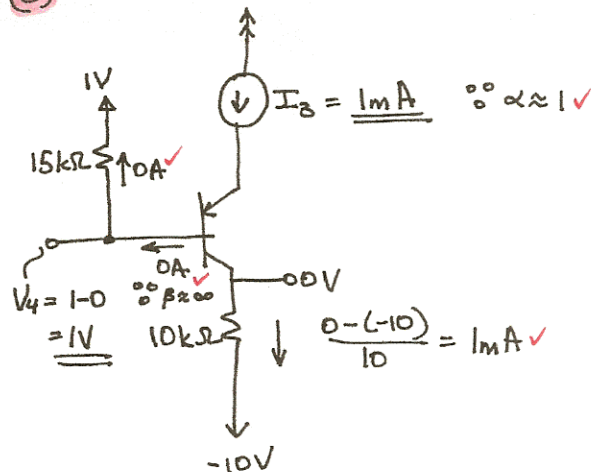
5.20

(a) $I_1 = \frac{10.7 - 0.7}{10} = 1 \text{ mA} \checkmark$

(b)

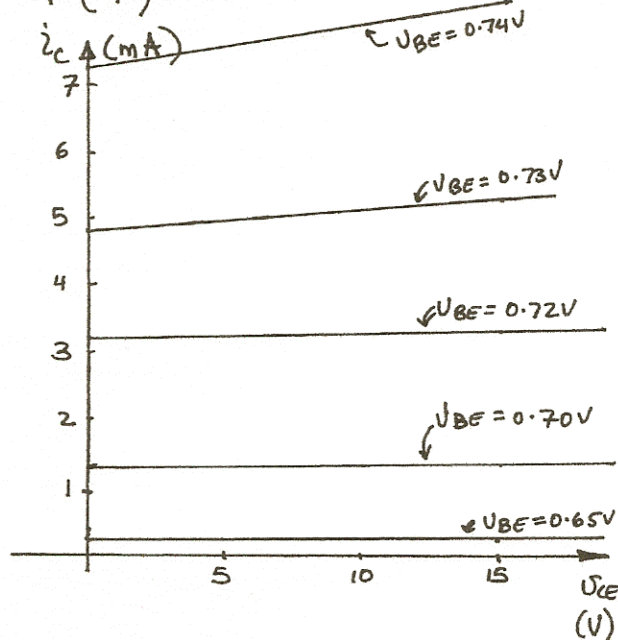


(c)



CONT

V_{BE} (V)	0.65	0.70	0.72	0.73	0.74
Intercept (mA)	0.2	1.45	3.22	4.80	7.16
Slope (mA/V)	0.002	0.015	0.032	0.048	0.072



5.38

$$r_o = \frac{1}{3 \times 10^{-5}} = \underline{\underline{33.3 \text{ k}\Omega}}$$

$$V_A = r_o I_C = 33.3 \times 10^3 \times 3 \times 10^{-3} = \underline{\underline{100 \text{ V}}}$$

$$r_o = \frac{V_A}{I_C} = \frac{100}{30} = \underline{\underline{3.3 \text{ k}\Omega}}$$

5.39

$$r_o = V_A / I_C = 200 / I_C$$

$$@ I_C = 1 \text{ mA} \quad r_o = \underline{\underline{200 \text{ k}\Omega}}$$

$$@ I_C = 100 \mu\text{A} \quad r_o = \frac{200}{0.1} = \underline{\underline{2.0 \text{ M}\Omega}}$$

5.40

$$V_{BE} = 0.72 \text{ V} \quad I_C = 1.8 \text{ mA} \quad V_{CE} = 2 \text{ V}$$

$$I_C = 2.4 \text{ mA} \quad V_{CE} = 14 \text{ V}$$

$$r_o = \frac{\Delta V_{CE}}{\Delta I_C} = \frac{14 - 2}{2.4 - 1.8} = \underline{\underline{20 \text{ k}\Omega}}$$

Near saturation $V_{CE} = 0.3 \text{ V}$

$$\therefore \frac{\Delta V_{CE}}{\Delta I_C} = \frac{0.3 - 2}{I_C - 1.8} = 20$$

$$I_C = \underline{\underline{1.72 \text{ mA}}}$$

calculating V_{CE} for $I_C = 2.0 \text{ mA}$

$$\frac{\Delta V_{CE}}{\Delta I_C} = r_o$$

$$\frac{V_{CE} - 2}{2 - 1.8} = 20 \Rightarrow V_{CE} = \underline{\underline{6 \text{ V}}}$$

Take the ratio of currents to find the Early Voltage (with Eq 5.36)

$$\frac{2.4}{1.8} = e^{\frac{V_{BE} - V_{BE}}{V_T}} \left(\frac{1 + 14/V_A}{1 + 2/V_A} \right)$$

$$= 1$$

$$2.4 + \frac{4.8}{V_A} = 1.8 + \frac{25.2}{V_A}$$

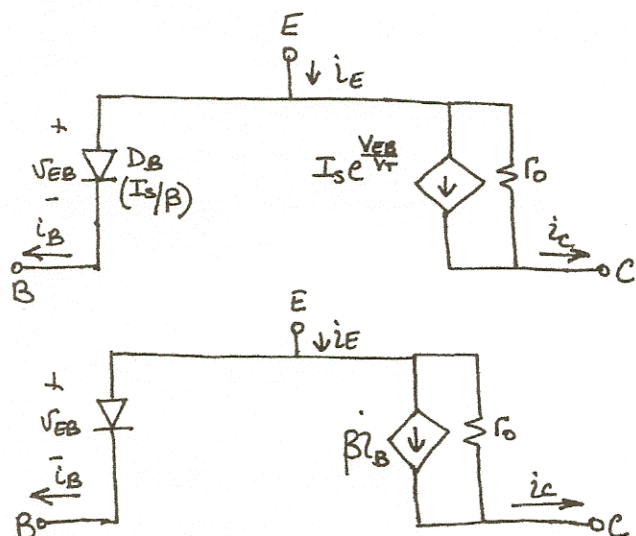
$$V_A = \underline{\underline{34 \text{ V}}}$$

$$r_o = \frac{V_A}{I_C'} \quad \text{where } I_C' \text{ is the current near saturation} \Leftrightarrow$$

$$= \frac{34}{1.72} \quad \text{active boundary. As calculated above } I_C' = 1.72 \text{ mA}$$

$$= \underline{\underline{19.8 \text{ k}\Omega}} \quad \leftarrow \approx \text{to the above calculation of } 20 \text{ k}\Omega.$$

5.41



5.42

Large signal or DC β :

$$h_{FE} = \frac{I_C}{I_B} = \frac{1.2 \text{ mA}}{8 \mu\text{A}} = \underline{150} \checkmark$$

$$\text{Small signal } h_{fe} = \frac{0.1 \text{ mA}}{0.8 \mu\text{A}} = \underline{125} \checkmark$$

$$r_o = \frac{V_A}{I_C} = \frac{100 \text{ V}}{1.2 \text{ mA}} = 83.3 \text{ k}\Omega \checkmark$$

$$\begin{aligned} \Delta I_C &= h_{fe} \Delta I_B + \frac{\Delta V_{CE}}{r_o} \\ &= 125 \times 2 \mu\text{A} + \frac{2}{83.3 \text{ k}\Omega} = 0.274 \text{ mA} \checkmark \end{aligned}$$

$$\therefore I_C = 1.2 \text{ mA} + \Delta I_C = \underline{1.474 \text{ mA}} \checkmark$$

5.43

	-55°C	25°C	125°C
$I_C = 100 \mu\text{A}$ $\beta \Rightarrow$	100	187	300
$I_C = 10 \text{ mA}$ $\beta \Rightarrow$	78	178	322

For $I_C = 100 \mu\text{A}$

$$\text{Temp coef below } 25^\circ\text{C} = \frac{187 - 100}{25 - 55} = \underline{1.09/^\circ\text{C}}$$

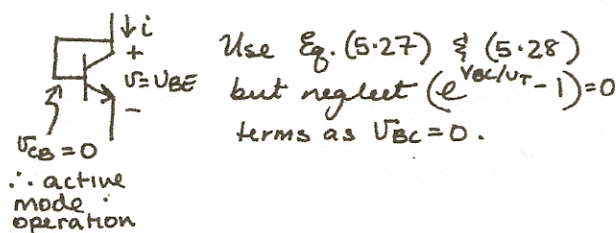
$$\text{Temp coef above } 25^\circ\text{C} = \frac{300 - 187}{125 - 25} = \underline{1.13/^\circ\text{C}}$$

For $I_C = 10 \text{ mA}$

$$\text{Temp coef below } 25^\circ\text{C} = \frac{178 - 78}{25 - 55} = \underline{1.25/^\circ\text{C}}$$

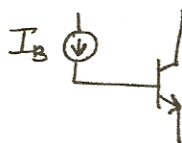
$$\text{Temp. coef above } 25^\circ\text{C} = \frac{322 - 178}{125 - 25} = \underline{1.44/^\circ\text{C}}$$

5.44



$$\begin{aligned} I &= I_C + I_B \\ &= I_S (e^{V_{BE}/V_T} - 1) + \frac{I_S}{\beta_F} (e^{V_{BE}/V_T} - 1) \\ &= I_S (e^{V_{BE}/V_T} - 1) \left(1 + \frac{1}{\beta_F} \right) \approx \frac{\beta_F + 1}{\beta_F} I_S e^{V_{BE}/V_T} \approx I_S e^{V_{BE}/V_T} \quad \text{Q.E.D.} \end{aligned}$$

5.45

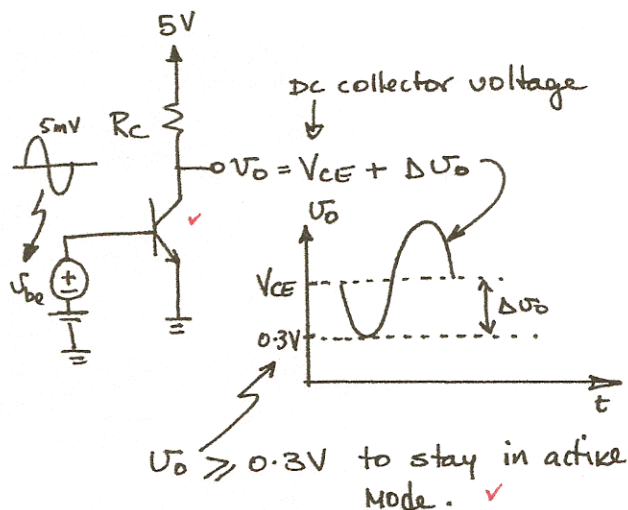


$$\begin{aligned} V_{CEsat} &= V_{CEoff} + I_{Csat} R_{Lsat} \\ &= V_T \ln \left(\frac{1}{\alpha_R} \right) \\ &= 0.025 \ln \frac{1}{0.2} = \underline{40.2 \text{ mV}} \end{aligned}$$

5.56

Maximize gain, not magnitude

Since we are assuming linear operation we don't have to go to $i_c = I_s e^{V_{BE}/V_T}$ equation. ✓



$$A_v = -\frac{I_c R_c}{V_T} = -\frac{V_{CC} - V_{CE}}{V_T} \quad \checkmark$$

On the verge of saturation

$$V_{CE} - \Delta V_O = 0.3V \quad \text{for linear operation}$$

peak value

$$\Delta V_O = A_v V_{be}$$

$$V_{CE} - |A_v V_{be}| = 0.3$$

$$(5 - I_c R_c) - |A_v \times 5 \times 10^{-3}| = 0.3$$

$$5 - |A_v V_T| - |A_v \times 5 \times 10^{-3}| = 0.3 \quad \checkmark$$

$$|A_v (0.025 + 0.005)| = 5 - 0.3 \quad \checkmark$$

$$|A_v| = 156.67 \quad \text{Note } A_v \text{ is negative.}$$

$$\therefore A_v = -156.67 \text{ V/V} \quad \checkmark$$

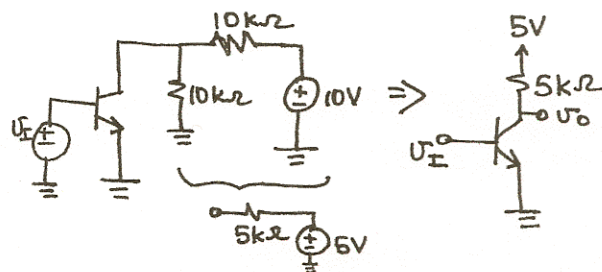
Now we can find the dc collector voltage. Refer to sketch of the output voltage, we see that

$$|\Delta V_O| = |A_v \times 0.005| \quad \checkmark$$

$$\therefore V_{CE} = 0.3 + |A_v| \times 0.005 \quad \checkmark$$

$$= \underline{1.08V} \quad \checkmark$$

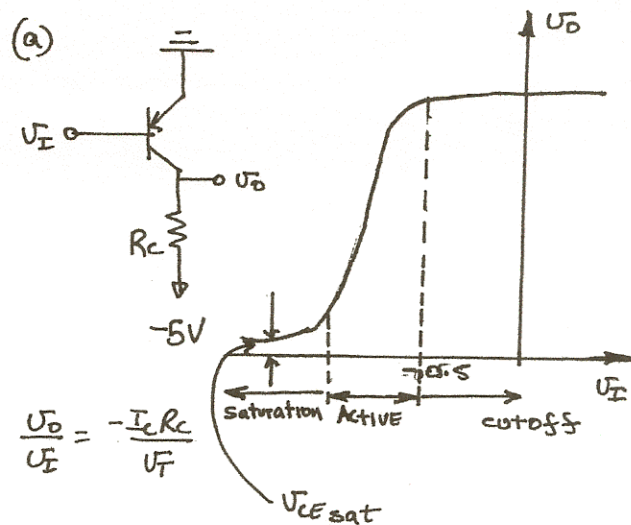
5.57



$$\frac{V_O}{V_I} = -\frac{I_c R_c}{V_T} = -\frac{0.5 \times 5}{0.026}$$

$$= \underline{-100 \text{ V/V}}$$

5.58

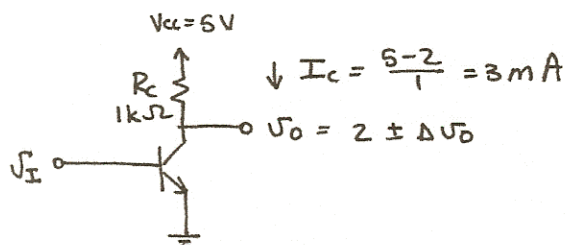


CONT.

But $V_{CE} = 0.5V$ & $\frac{I_C R_C}{V_T} = 100$ as shown above.

$$\begin{aligned} \therefore A_v &= \frac{-100}{1 + \frac{2.5}{100 + 2.5}} \\ &= \underline{\underline{-97.7 V/V}} \end{aligned}$$

5.60



Small signal voltage gain

$$A_v = -\frac{I_C R_C}{V_T} = \frac{-3 \times 1}{0.025} = \underline{\underline{-120 V/V}}$$

If we assume linear operation around the bias point we can use A_v .

$$\Delta V_O = -120 \times 5 \times 10^{-3} = \underline{\underline{-0.6V}} \quad \text{for } \Delta V_{BE} = 5mV$$

$$\Delta V_O = 120 \times 5 \times 10^{-3} = \underline{\underline{0.6V}} \quad \text{for } \Delta V_{BE} = -5mV$$

Using the transistor exponential characteristics as in Example 5.2:

for $\Delta V_{BE} = 5mV$:

$$\frac{I_C}{3mA} = e^{\Delta V_{BE}/V_T} = e^{5/25}$$

$$I_C = 3.66mA$$

$$V_O = 5 - 3.66 = 1.34V$$

$$\Delta V_O = 1.34 - 2 = \underline{\underline{-0.66V}}$$

For $\Delta V_{BE} = -5mV$

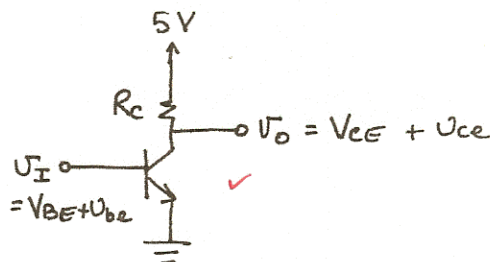
$$I_C = 3 \times e^{-5/25} = 2.46mA$$

$$V_O = 5 - 2.46 \times 1 = 2.54V$$

$$\Delta V_O = 2.54 - 2 = \underline{\underline{0.54V}}$$

$\Delta V_{BE} (mV)$	$\Delta V_O (V)$ Exponential	$\Delta V_O (V)$ Linear
+0.5	-0.66	-0.6
-0.5	+0.54	+0.6

5.61



(a) For maximum gain you would bias at the largest current since $A_v = -I_C R_C / V_T$. This also means you would bias at the edge of saturation $A_v = \frac{-V_{CC} - V_{CEsat}}{V_T}$

$$\begin{aligned} &= \frac{-(5 - 0.3)}{0.025} = \frac{-4.7}{0.025} \\ &= \underline{\underline{-188 V/V}} \end{aligned}$$

However any signal swing at the output would automatically drive it into saturation. ✓

(b) For $A_v = -100 V/V$

$$A_v = \frac{V_{CC} - V_{CE}}{V_T} = \frac{5 - V_{CE}}{V_T} = 100 \quad \checkmark$$

$$V_{CE} = \underline{\underline{2.5V}} \quad \checkmark$$

CONT.

(c) For a dc collector current of 0.5mA

$$R_c = \frac{5-2.5}{0.5} = \underline{\underline{5\text{ k}\Omega}} \checkmark$$

(d) $I_s = 10^{-15}\text{A} \Rightarrow$

$$I_c = I_s e^{V_{BE}/V_T} \checkmark$$

$$0.5 \times 10^{-3} = 10^{-15} e^{V_{BE}/0.025} \checkmark$$

$$V_{BE} = \underline{\underline{0.673\text{V}}} \checkmark$$

(e) If we assume linear operation we can use A_v to find the output change for $U_{be} = 5\text{mV}$

$$U_{ce} = A_v U_{be} = -100 \times 0.005 \checkmark$$

$$= -0.5\text{V} \sim \text{peak sine wave.}$$

$\therefore$ the output is a 0.5V p sine wave $\checkmark$

(f) for $U_{ce} = 0.5$

$$i_c = \frac{0.5}{5} = \underline{\underline{0.1\text{mA peak}}} \checkmark$$

This current is superimposed on I_c .

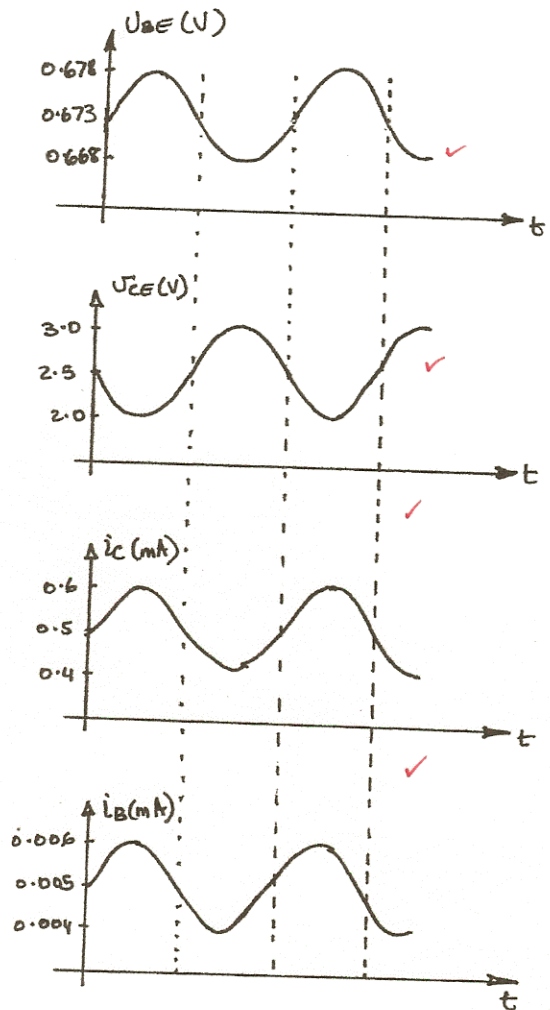
(g) $I_B = I_c / \beta = \frac{0.5}{100} = \underline{\underline{0.005\text{mA}}} \checkmark$

$$i_b = \frac{i_c}{\beta} = \frac{0.1}{100} = \underline{\underline{0.001\text{mA}}} \checkmark$$

(h) $r_{in} = \frac{U_{be}}{i_b} = \frac{0.005}{0.001 \times 10^{-3}}$

$$= \underline{\underline{5\text{ k}\Omega}} \checkmark$$

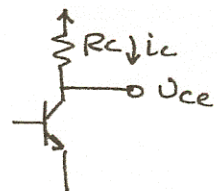
(i) see sketches that follow:



5.62

Eq (5.56)

$$A_v = \frac{U_{ce}}{U_{be}} = -\frac{I_c R_c}{V_T}$$



But $U_{ce} = -i_c R_c$

$$\therefore -\frac{i_c R_c}{U_{be}} = -\frac{I_c R_c}{V_T}$$

Now $g_m = \frac{\text{output current}}{\text{input voltage}} = \frac{i_c}{U_{be}}$

$$\therefore g_m R_c = \frac{I_c R_c}{V_T}$$

$$\underline{\underline{g_m = I_c / V_T}}$$

load line between points N and M. To obtain the coordinates of point M, we solve the load line and line L_2 to find the intersection M and the load line and line L_3 to find N:

For Point M:

$$i_c = 8 + \frac{8}{100} V_{CE} \quad \& \quad i_c = 10 - V_{CE}$$

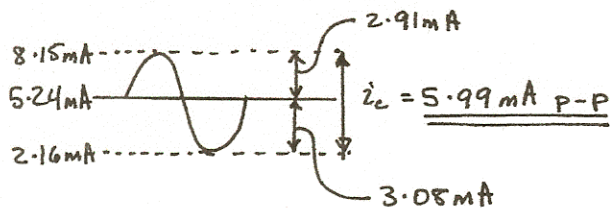
$$\therefore i_{c|M} = 8.15 \text{ mA} \quad V_{CE|M} = 1.85 \text{ V}$$

For Point N:

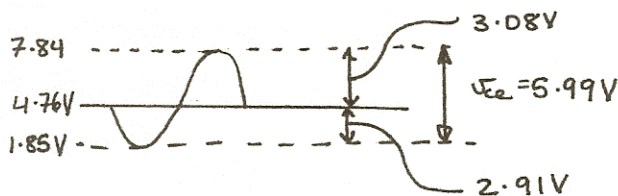
$$i_c = 2 + 0.02 V_{CE} \quad \& \quad i_c = 10 - V_{CE}$$

$$V_{CE|N} = 7.84 \text{ V} \quad i_{c|N} = 2.16 \text{ mA}$$

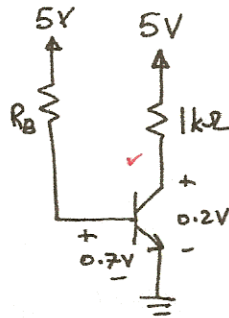
Thus the collector current varies as follows



And the collector voltage varies as:



5.65



$$\frac{\beta_F}{\beta_{\text{forced}}} = \text{overdrive factor} = 10$$

$$\therefore \beta_{\text{forced}} = \frac{\beta_F}{10} = \frac{20}{10} = 2$$

for $V_{CE\text{sat}} = 0.2 \text{ V}$

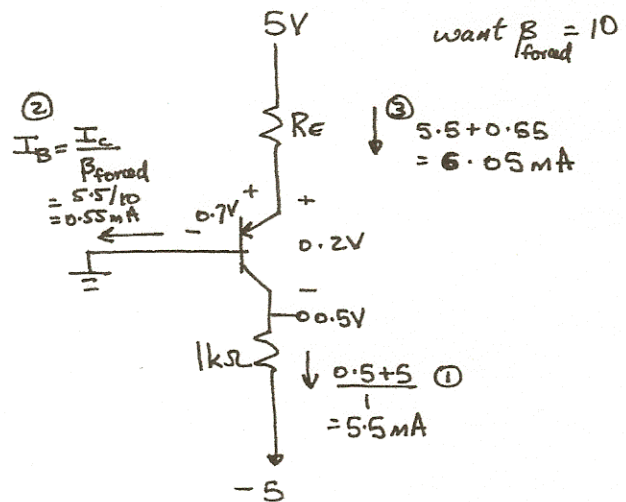
$$5 - I_{\text{csat}} \times 1 = 0.2$$

$$I_{\text{csat}} = 5 - 0.2 = 4.8 \text{ mA}$$

$$I_B = \frac{I_{\text{csat}}}{\beta_{\text{forced}}} = \frac{4.8}{2} = 2.4 \text{ mA}$$

$$\therefore R_B = \frac{5 - 0.7}{2.4} = \frac{4.3}{2.4} = 1.8 \text{ k}\Omega$$

5.66



$$R_E = \frac{5 - 0.7}{6.05} = 710 \Omega$$

$$V_E = \underline{2.49V}$$

$$V_C = 2.49 + 0.2 = \underline{2.69V}$$

$$V_B = V_E + 0.7 = \underline{3.19V}$$

$$\text{Check: } I_C = \frac{5 - 2.69}{1} = 2.31 \text{ mA}$$

$$I_B = \frac{5 - 3.19}{10} = 0.181 \text{ mA}$$

$$\frac{I_C}{I_B} = \frac{2.31}{0.181} = 12.76 < 100$$

Hence
we are in
saturation as
assumed!

(C) $R_B = 1k\Omega$ - expect saturation
- use circuit in (b)

$$I_B = \frac{5 - (V_E + 0.7)}{R_B} = \frac{4.3 - V_E}{1}$$

$$I_C = \frac{5 - (V_E + 0.2)}{1} = \frac{4.8 - V_E}{1}$$

$$I_E = I_B + I_C = V_E$$

$$4.3 - V_E + 4.8 - V_E = V_E$$

$$V_E = \underline{3V}$$

$$V_B = \underline{3.7V}$$

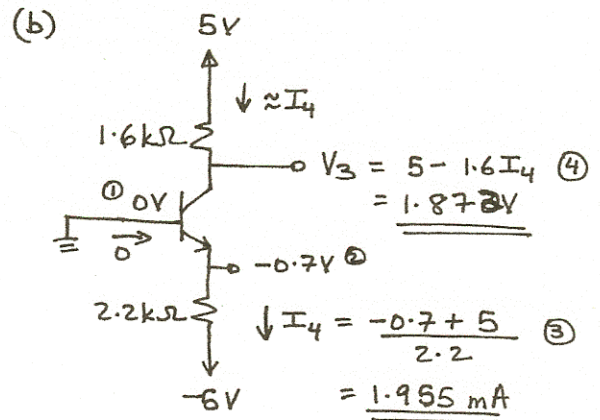
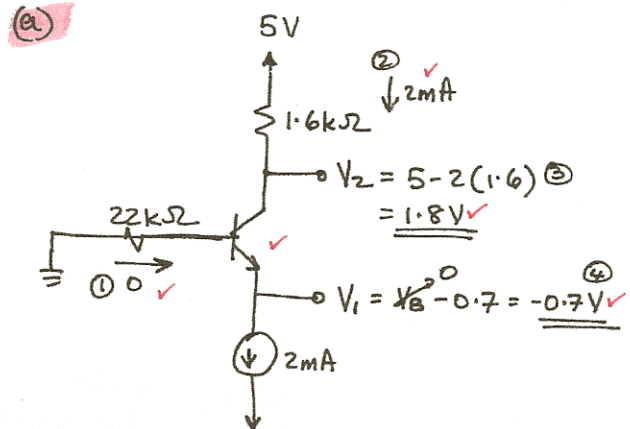
$$V_C = \underline{3.2V}$$

$$\text{Check } I_B = 4.3 - 3 = 1.3 \text{ mA}$$

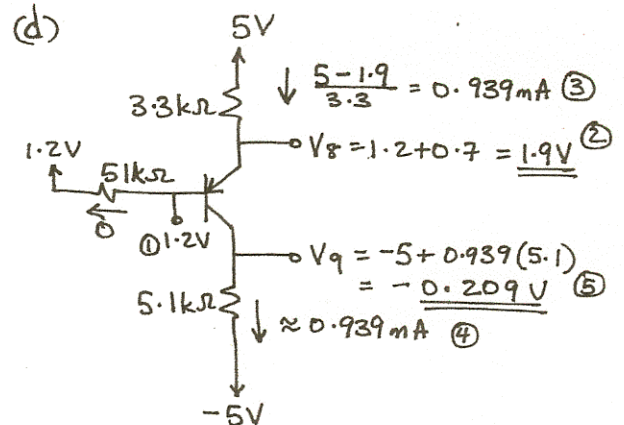
$$I_C = 4.8 - 3 = 1.8 \text{ mA}$$

$$\frac{I_C}{I_B} = \frac{1.8}{1.3} = 1.4 < 100 \therefore \text{SATURATION AS ASSUMED}$$

5.79

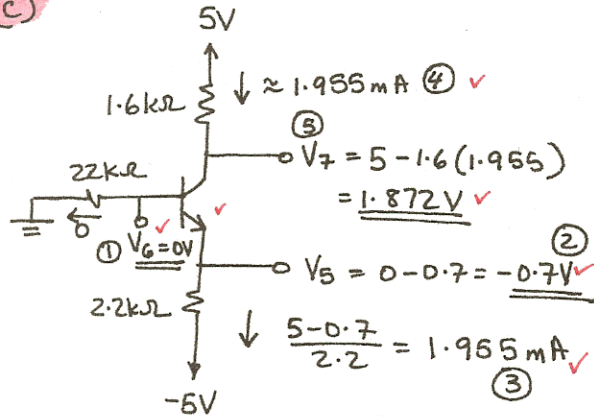


see below for part (c)

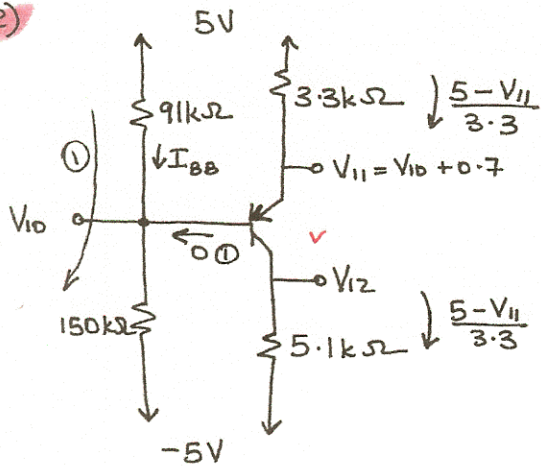


CONT.

(c)



(e)



Loop ①

$$5 - 91I_{BB} - 150I_{BB} + 5 = 0 \quad \checkmark$$

$$I_{BB} = \frac{10}{91 + 150} \quad \checkmark$$

$$V_{10} = -5 + 150I_{BB} \quad \checkmark$$

$$= -5 + \frac{150}{91 + 150} \times 10$$

$$= 1.224V \quad \checkmark$$

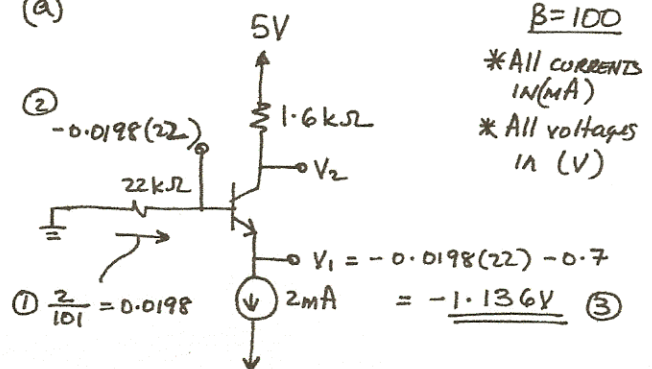
$$V_{11} = V_{10} + 0.7 = 1.924V \quad \checkmark$$

$$\therefore I_C \approx I_E = \frac{5 - V_{11}}{3.3} \quad \checkmark$$

$$V_{12} = -5 + \left(\frac{5 - V_{11}}{3.3}\right) 5.1 = -0.246V \quad \checkmark$$

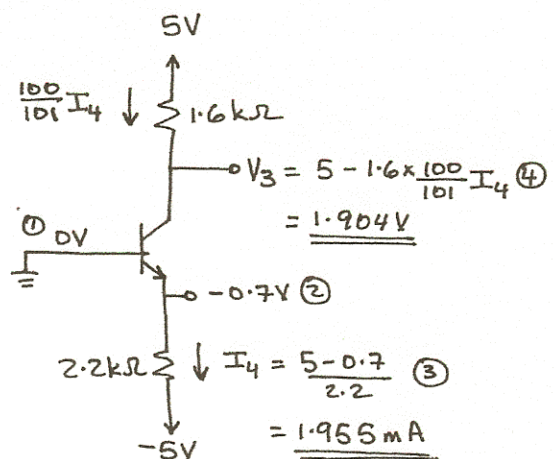
5.80

(a)

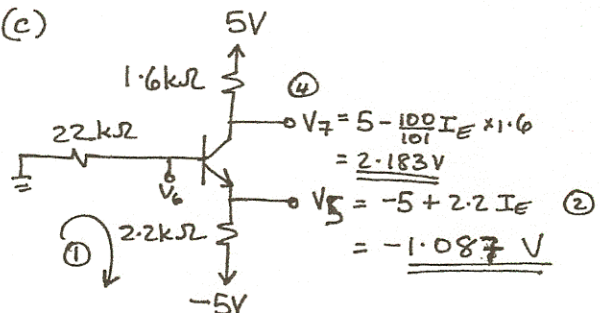


$$V_2 = 5 - 2\left(\frac{100}{101}\right) 1.6 = 1.832V$$

(b)



(c)



$$\text{Loop ① } 0 - \frac{I_E}{101} 22 - 0.7 - 2.2 I_E + 5 = 0$$

$$I_E = 1.778mA$$

$$V_6 = V_5 + 0.7 = -0.387V$$

CONT

For I_C : $I_C = I_S e^{V_{BE}/V_T}$
 for $V_{BE} = 0.690 \rightarrow I_C = 1 \text{ mA}$
 $\Rightarrow I_S = 1.032 \times 10^{-15}$

for $V_{BE} = 0.678 \rightarrow I_C = 0.618 \text{ mA}$
 $V_{BE} = 0.702 \rightarrow I_C = 1.62 \text{ mA}$

I_C ranges from 0.618 mA to 1.62 mA .

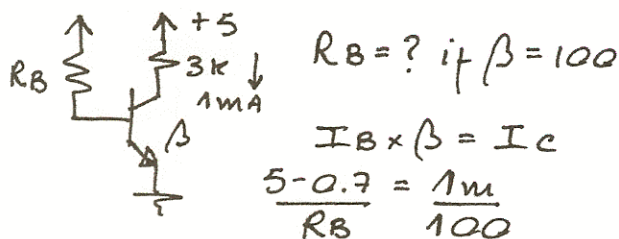
③ If $R_C = 3 \text{ K}\Omega$

$V_{CE} = 5 - 3 \text{ K} \times 0.62 \text{ mA} = 3.14 \text{ V}$

$V_{CE} = 5 - 3 \text{ K} \times 1.62 \text{ mA} = 0.14 \text{ V}$

This circuit is too sensitive to parameter variations as shown here for a 1% resistor tolerance.

5.89



$\rightarrow R_B = 430 \text{ K}\Omega$

$V_{CE} = 5 \text{ V} - 3 \text{ K} \cdot 1 \text{ mA} = 2 \text{ V}$

If $\beta = 50$: $I_C = \frac{5 - 0.7}{430 \text{ K}} \times 50$

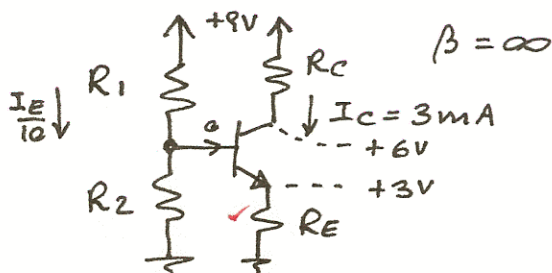
$I_C = 0.50 \text{ mA}$

$\Rightarrow V_{CE} = 5 - 3 \text{ K} \times 0.5 \text{ mA} = +3.5 \text{ V}$

If $\beta = 150$: $I_C = 1.5 \text{ mA}$
 $V_{CE} = 0.5 \text{ V}$

This design is too sensitive to variations of β .

5.90



$R_C = \frac{3 \text{ V}}{3 \text{ mA}} = 1 \text{ K}\Omega$

$R_E = \frac{3 \text{ V}}{3 \text{ mA}} = 1 \text{ K}\Omega$

$V_B = 0.7 + 3 = 3.7 \text{ V}$

$R_1 = \frac{9 - 3.7}{I_{E/10}} = 17.7 \text{ K}\Omega$

$9 \text{ V} = (R_1 + R_2) \frac{I_E}{10} \rightarrow R_2 = 12.3 \text{ K}\Omega$

Choose suitable 5% resistors

$R_1 = 17.7 \text{ K} \rightarrow 18 \text{ K}\Omega$

$R_2 = 12.3 \text{ K} \rightarrow 13 \text{ K}\Omega$

$R_E = R_C = 1 \text{ K}$

$V_{BB} = \frac{9 \times 13}{18 + 13} = 3.77 \text{ V}$

For these values of R and $\beta = 90$: $R_B = 18 \parallel 13 = 7.55 \text{ K}\Omega$

$I_E = \frac{3.77 - 0.7}{1 \text{ K} + \frac{7.55 \text{ K}}{91}} = 2.83 \text{ mA}$

$V_E = (2.83)(1) = 2.83 \text{ V}$

$\alpha = 0.989 \Rightarrow I_C = 2.80 \text{ mA}$

If R_E is reduced by $\sim \frac{7.55 \text{ K}}{91}$

$\rightarrow R_E = 910 \Omega$
 $\Rightarrow I_E = 3.09 \text{ mA}$

$I_C = 3.05 \text{ mA}$
 $V_B = (2.83)(1) + 0.7 = 3.53 \text{ V}$

$V_C = 9 - (2.8)(1) = 6.2 \text{ V}$

Selection of a value for R_c :

The voltage gain is directly proportional to R_c ,

$$\begin{aligned}\frac{V_o}{V_s} &= \frac{V_e}{V_s} \cdot \frac{V_o}{V_e} \\ &= \frac{R_{in}}{R_s + R_{in}} \cdot \frac{\alpha R_c}{r_e} \\ &\approx \frac{100}{100 + 100} \cdot \frac{R_c}{0.1} \\ &= 5R_c, R_c \text{ in } k\Omega.\end{aligned}$$

For an emitter-base signal as large as 10mV, the signal at the collector will be $g_m R_c \times 0.010$ volts. Thus the maximum collector voltage in the positive direction will be:

$$\begin{aligned}V_{c|max} &= V_c + 0.01 g_m \cdot R_c \\ &= -10 + I_e R_c + 0.01 \times \frac{1}{0.1} \times R_c \\ &= -10 + 0.25 R_c + 0.1 R_c \\ &= -10 + 0.35 R_c\end{aligned}$$

To prevent saturation, $V_{c|max} \leq V_B$ which is 0V. Thus to obtain maximum gain while allowing an emitter-base signal as large as 10mV and at the same time keeping the transistor in the active mode we select R_c from:

$$\begin{aligned}-10 + 0.35 R_c &= 0 \\ \Rightarrow R_c &= \underline{\underline{28.6 k\Omega}}\end{aligned}$$

$$\text{Voltage gain} = \frac{V_o}{V_s} = 5R_c = 143 V/V$$

5.124

Refer to Fig P5.124
For large β , the DC base current will be ~ 0 ✓
Thus the DC voltage at the base can be found directly using the voltage divider rule ✓

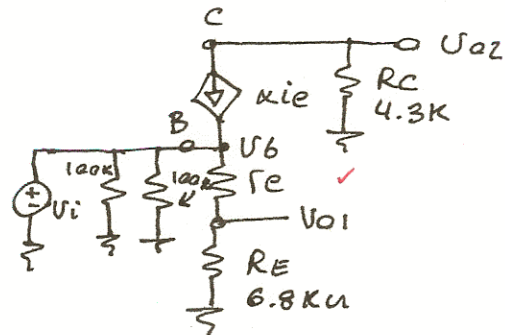
$$V_B = 15 \cdot \frac{100}{100 + 100} = 7.5 V \checkmark$$

$$V_{BE} = 0.7$$

$$V_E = 7.5 - 0.7 = 6.8 V \checkmark$$

$$\rightarrow I_E = \frac{6.8 V}{6.8 k\Omega} = 1 mA \checkmark$$

$I_C = I_E$



$$V_B = V_i \checkmark$$

$$\rightarrow \frac{V_{o1}}{V_i} = \frac{R_E}{R_E + r_e} \checkmark \text{ Q.E.D.}$$

Also,

$$i_e = \frac{V_B}{r_e + R_E} = \frac{V_i}{r_e + R_E} \checkmark$$

and,

$$\begin{aligned}V_{o2} &= -\alpha i_e R_c \\ &= -\frac{\alpha R_c V_i}{r_e + R_E} \checkmark\end{aligned}$$

Thus,

$$\frac{V_{o2}}{V_i} = -\frac{\alpha R_c}{R_E + r_e} \checkmark \text{ Q.E.D.}$$

CONT.

Substituting $r_e = \frac{V_T}{I_E} = 25\Omega$

and $R_E = 6.8k\Omega$, $R_C = 4.3k\Omega$
and $\alpha \approx 1$ gives

$$\frac{V_{o1}}{V_i} = \frac{6.8}{0.025 + 6.8} = \underline{\underline{0.996 \text{ V/V}}}$$

$$\frac{V_{o2}}{V_i} = -\frac{4.3}{6.8 + 0.025} = \underline{\underline{-0.63 \text{ V/V}}}$$

If the node labeled V_{o2} is connected to ground:
 $R_E = 0$ ✓

$$\frac{V_{o2}}{V_i} = -\alpha \frac{R_C}{r_e} \checkmark$$

5.125

If: $R_i = 10k\Omega$, $A_{vo} = 100 \text{ V/V}$
 $R_o = 100\Omega$, $R_{sig} = 2k\Omega$ and
 $R_{in} = 8k\Omega$ when $R_L = 1k\Omega$
then:

$$G_m = \frac{A_{vo}}{R_o} = \frac{100}{100} = 1 \text{ A/V}$$

$$A_v = A_{vo} \cdot \frac{R_L}{R_L + R_o} = 100 \times \frac{1k}{1k + 100} = \underline{\underline{91 \text{ V/V}}}$$

$$G_{vo} = \frac{R_i}{R_i + R_{sig}} \cdot A_{vo} = \frac{10k}{10k + 2k} \times 100 = \underline{\underline{83.3 \text{ V/V}}}$$

$$G_v = \frac{R_{in}}{R_{in} + R_{sig}} \times A_{vo} \times \frac{R_L}{R_L + R_o}$$

$$= \frac{8k}{8k + 2k} \times 100 \times \frac{1k}{1k + 100} = \underline{\underline{72.7 \text{ V/V}}}$$

$$R_{out} = \frac{G_{vo}}{G_v} \cdot R_L - R_L = \frac{83.3}{72.7} \times 1k - 1k$$

$$= \underline{\underline{146\Omega}}$$

$$A_i = \frac{V_o / R_L}{V_i / R_{in}} = A_v \cdot \frac{R_{in}}{R_L} = 91 \times \frac{8k}{1k}$$

$$= \underline{\underline{728 \text{ A/A}}}$$

5.126

Refer to Fig. P5.126

$$R_i = 900k\Omega$$

$$A_{vo} = 10 \text{ V/V}$$

$$R_o = 1.43k\Omega$$

$$R_{in} = 400k\Omega \text{ when } R_L = 10k\Omega$$

$$(a) i_i \equiv V_i / R_{in}$$

$$\Rightarrow \frac{V_i}{R_{in}} = \frac{V_i}{R_i} - f \cdot i_o$$

$$\text{where } i_o = \frac{A_{vo} V_i}{R_o + R_L}$$

$$\rightarrow \frac{V_i}{R_{in}} = \frac{V_i}{R_i} - f \cdot \frac{A_{vo} V_i}{R_o + R_L}$$

Solving for f :

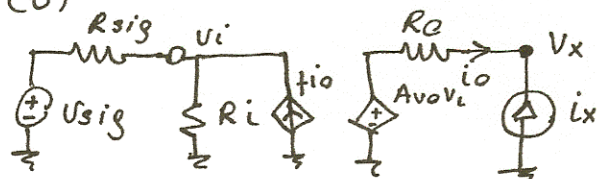
$$f = \left(\frac{1}{R_i} - \frac{1}{R_{in}} \right) \cdot \frac{R_o + R_L}{A_{vo}}$$

Thus,

$$f = \left(\frac{1}{900k} - \frac{1}{400k} \right) \cdot \frac{(1.43k + 10k)}{10}$$

$$f = \underline{\underline{-1.6 \times 10^{-3}}}$$

(b)



$$R_{out} = \frac{V_x}{i_x} \bigg|_{V_{sig}=0}$$

If $V_{sig}=0$: on the left hand side

$$V_i = f \cdot i_o (R_{sig} \parallel R_i)$$

$$V_i = (-1.6 \times 10^{-3} \times (100k \parallel 900k)) i_o$$

$$= -144 \cdot i_o$$

On the right hand side:

$$V_x = R_o i_x + A_{vo} V_i$$

$$= R_o i_x + A_{vo} (-144 i_o)$$

$$= R_o i_x + A_{vo} (+144) i_x$$

CONT.

5.129

$$I_C = 0.2 \text{ mA} \Rightarrow r_e = 123.76 \Omega$$

$$R_i = (\beta + 1)(r_e + R_E)$$

$$= (101)(123.76 + 125) = \underline{25.1 \text{ K}\Omega}$$

$$\frac{U_o}{U_s} = \frac{-\alpha R_C}{r_e + R_E} \times \frac{R_i}{R_i + R_s}$$

$$= \frac{-100 \times 24 \text{ K}}{101(123.76 + 125)} \times \frac{25.1 \text{ K}}{25.1 \text{ K} + 10 \text{ K}}$$

$$= \underline{-68.30 \text{ V/V}}$$

$$R_o = R_C = \underline{24 \text{ K}\Omega}$$

With $10 \text{ K}\Omega$ load

$$\frac{U_o}{U_s} = -68.30 \times \frac{10}{10 + 24} = \underline{-20 \text{ V}}$$

Without R_E $V_{\pi} \leq 5 \text{ mV}$

$$V_{\pi} = \frac{(\beta + 1)r_e}{(\beta + 1)r_e + R_s} \cdot V_s$$

$$= \frac{(101) \cdot (123.76)}{(101) \cdot (123.76) + (10 \text{ K})} \cdot V_s \leq 5 \text{ mV}$$

$$\Rightarrow V_s \leq \underline{9 \text{ mV}}$$

With R_E

$$V_{\pi} = \frac{(\beta + 1)r_e}{(\beta + 1)(r_e + R_E) + R_s} \cdot V_s \leq 5 \text{ mV}$$

$$V_s \leq 5 \text{ mV} \left[\frac{(101)(123.76 + 125) + 10 \text{ K}}{101 \times 123.76} \right]$$

$$V_s \leq \underline{14 \text{ mV}}$$

5.130

Refer to Fig. P5.130

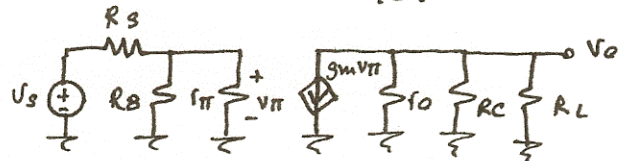
$$I_E = \frac{V_{BB} - V_{BE}}{R_E + R_B / (\beta + 1)}$$

$$\text{where, } V_{BB} = V_{CC} \cdot \frac{R_2}{R_1 + R_2}$$

$$= 9 \cdot \frac{15}{27 + 15} = 3.21 \text{ V}$$

$$R_B = R_1 \parallel R_2 = 15 \parallel 27 = 9.64 \text{ K}\Omega$$

$$\text{Thus, } I_E = \frac{3.21 - 0.7}{\frac{1.2}{101} + 9.64} = \underline{1.94 \text{ mA}}$$



$$g_m = \frac{I_C}{V_T} = \frac{0.99 \times 1.94}{0.025} = 76.8 \frac{\text{mA}}{\text{V}}$$

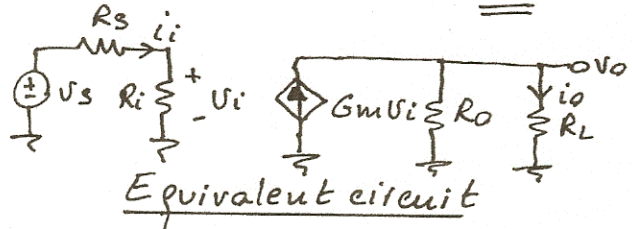
$$r_{\pi} = \frac{\beta}{g_m} = \frac{100}{76.8} = 1.3 \text{ K}\Omega$$

$$r_o = \frac{V_A}{I_C} = \frac{100}{0.99 \times 1.94} = 52.1 \text{ K}\Omega$$

$$R_i = R_B \parallel r_{\pi} = 9.64 \parallel 1.3 = \underline{1.15 \text{ K}\Omega}$$

$$G_m = -g_m = -\underline{76.8 \frac{\text{mA}}{\text{V}}}$$

$$R_o = R_C \parallel r_o = 2.2 \parallel 52.1 = \underline{2.11 \text{ K}\Omega}$$



$$A_V = \frac{U_o}{U_s} = \frac{U_i}{U_s} \cdot \frac{U_o}{U_i}$$

$$= \frac{R_i}{R_s + R_i} \cdot \frac{G_m (R_o \parallel R_L) U_i}{U_i}$$

$$= \frac{-1.15}{10 + 1.15} \times 76.8 \times (2.11 \parallel 2)$$

$$= \underline{-8.13 \text{ V/V}}$$

$$A_i = \frac{i_o}{i_i} = \frac{U_o \cdot R_L}{U_s (R_s + R_i)}$$

CONT.

$$\begin{aligned} \rightarrow A_i &= \frac{V_o}{V_s} \cdot \frac{R_s + R_i}{R_L} \\ &= -8.13 \times \frac{(10 + 1.15)}{2} \\ &= \underline{\underline{-45.3 \text{ A/A}}} \end{aligned}$$

5.131

Refer to Fig. P5.130.
 $V_{CC} = 9V$ $V_{BB} = \frac{1}{3} V_{CC} = 3V$

Neglecting the base current,
 $R_1 + R_2 = \frac{9}{0.2} = 45 \text{ k}\Omega$

$$\begin{aligned} \frac{R_2}{R_1 + R_2} &= \frac{1}{3} \\ \Rightarrow R_2 &= 15 \text{ k}\Omega, R_1 = 30 \text{ k}\Omega \\ R_B &= R_1 \parallel R_2 = \frac{30 \times 15}{45} = 10 \text{ k}\Omega \end{aligned}$$

$$I_E = \frac{V_{BB} - V_{BE}}{R_E + \frac{R_B}{\beta + 1}}$$

$$2 = \frac{3 - 0.7}{R_E + 10/101} \Rightarrow R_E = \underline{\underline{1.05 \text{ k}\Omega}}$$

Use $R_E = 1 \text{ k}\Omega$

The resulting I_E will be

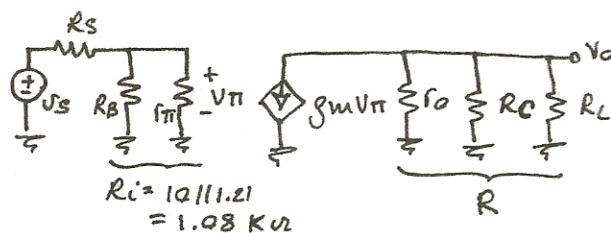
$$I_E = \frac{3 - 0.7}{1 + 10/101} = 2.09 \text{ mA}$$

$$I_C = \alpha I_E = 0.99 \times 2.09 = 2.07 \text{ mA}$$

$$g_m = \frac{I_C}{V_T} = \frac{2.07}{0.025} = 82.9 \frac{\text{mA}}{\text{V}}$$

$$r_{\pi} = \frac{\beta}{g_m} = \frac{100}{82.9} = 1.21 \text{ k}\Omega$$

$$r_o = \frac{V_A}{I_C} = \frac{100}{2.07} = 48.3 \text{ k}\Omega.$$



$$\begin{aligned} \frac{V_o}{V_s} &= \frac{V_{\pi}}{V_s} \cdot \frac{V_o}{V_{\pi}} = \frac{R_i}{R_s + R_i} \cdot \frac{-g_m V_{\pi} R}{V_{\pi}} \\ &= \frac{-1.08}{10 + 1.08} \times 82.9 \times R \end{aligned}$$

To obtain $\frac{V_o}{V_s} = -8 \frac{\text{V}}{\text{V}}$ we use:

$$R = \frac{8 \times 11.08}{1.08 \times 82.9} = 0.99 \text{ k}\Omega$$

$$\begin{aligned} \text{Now } R &= r_o \parallel R_C \parallel R_L \\ 0.99 &= 48.3 \parallel R_C \parallel 2 \\ \Rightarrow R_C &= 2.04 \text{ k}\Omega \end{aligned}$$

Use $R_C = 2 \text{ k}\Omega$

Check: $V_C = 9 - 2.07 \times 2 = 4.86 \text{ V}$
 while $V_B \approx 3 \text{ V}$. Thus in active mode as assumed.

5.132

Refer to Fig. P5.130

$$V_{BB} = 9 \cdot \frac{47}{82 + 47} = 3.28 \text{ V}$$

$$R_B = 47 \parallel 82 = 29.88 \text{ k}\Omega$$

$$I_E = \frac{3.28 - 0.7}{3.6 + \frac{29.88}{101}} = 0.66 \text{ mA}$$

$$I_C = 0.99 \times 0.66 = 0.65 \text{ mA}$$

$$g_m = \frac{0.65}{0.025} = 26 \frac{\text{mA}}{\text{V}}$$

$$r_{\pi} = \frac{100}{26} = 3.85 \text{ k}\Omega$$

$$r_o = \frac{100}{0.66} = 151.5 \text{ k}\Omega$$

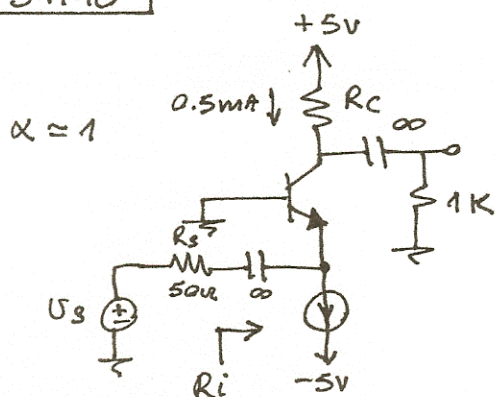
CONT.

5.139

$V_{CC} =$
 $R_C = 10\text{ k}\Omega$
 $R_{B1} = 100\text{ k}\Omega$
 $R_{B2} = 10\text{ k}\Omega$
 $R_E = 25\text{ m}\Omega = 100\text{ }\Omega$
 $R_s = 100\text{ k}\Omega$
 C_{be}
 V_s
 I
 V_o
 $-V_{EE}$

$R_i = r_e$
 $r_e = \frac{25\text{ m}}{I} = 100$
 $I = \frac{25\text{ m}}{100} = 0.25\text{ mA}$
 $\frac{V_o}{V_s} = -\alpha \frac{(R_C || R_L)}{R_s + r_e}$
 assuming $\alpha = 1$

5.140



$$V_{C_{min}} = V_C - 0.01 g_m (R_C || 1K)$$

$$\rightarrow 0 = V_c - 0.01 \times 20 \text{ (Re//1)}$$

$$R_c = \frac{4.3 + \sqrt{4.3^2 + 10}}{1}$$

$(0.45 - 0.18)V$ to $(0.45 + 0.18)V$
i.e. from $0.27V$ to $0.63V$

Thus, $\frac{V_o}{V_s} = 19.8 \times 0.5 = \underline{\underline{9.9 \text{ V/V}}}$

$$\text{for } \beta = 40, I_E = \frac{8.3}{1 + \frac{100}{41}} = \underline{\underline{2.41 \text{ mA}}}$$

$$V_E = 1 \times 2.41 = \underline{\underline{2.41 \text{ V}}}$$

$$V_B = 2.41 + 0.7 = \underline{\underline{3.11 \text{ V}}}$$

$$\text{For } \beta = 200, I_E = \frac{8.3}{1 + \frac{100}{201}} = \underline{\underline{5.54 \text{ mA}}}$$

$$V_E = + \underline{\underline{5.54 \text{ V}}}$$

$$V_B = + \underline{\underline{6.24 \text{ V}}}$$

$$(b) R_i = 100 \text{ K}\Omega \parallel (\beta + 1) [r_e + (1 \parallel 1)]$$

$$= 100 \parallel (\beta + 1) [r_e + 0.5]$$

$$\text{For } \beta = 40, I_E = 2.41 \text{ mA}$$

$$\rightarrow r_e = 10.37 \Omega$$

$$\text{thus } R_i = 100 \parallel 41 \times (0.01037 + 0.5)$$

$$= 100 \parallel 21$$

$$= \underline{\underline{17.30 \Omega}}$$

$$\text{For } \beta = 200, I_E = 5.54 \text{ mA}$$

$$\rightarrow r_e = 4.51 \Omega$$

$$\text{thus } R_i = 100 \parallel 201 (0.0045 + 0.5)$$

$$= 100 \parallel 101.4$$

$$= \underline{\underline{50.3 \text{ K}\Omega}}$$

$$(c) \frac{V_o}{V_s} = \frac{V_b}{V_s} \cdot \frac{V_o}{V_b}$$

$$= \frac{R_i}{R_s + R_i} \cdot \frac{(1 \parallel 1)}{(1 \parallel 1) + r_e}$$

$$\text{For } \beta = 40,$$

$$\frac{V_o}{V_s} = \frac{17.3}{10 + 17.3} \times \frac{0.5}{0.5 + 0.01037}$$

$$= \underline{\underline{0.621 \text{ V/V}}}$$

$$\text{For } \beta = 200,$$

$$\frac{V_o}{V_s} = \frac{50.3}{10 + 50.3} \cdot \frac{0.5}{0.5 + 0.0045}$$

$$= \underline{\underline{0.827 \text{ V/V}}}$$

5.144

Refer to Fig. P5.144

$$I_E = \frac{5 - 0.7}{3.3 + \frac{100}{101}} = \underline{\underline{1.00 \text{ mA}}}$$

$$r_e = \frac{25}{1.00} = 25 \Omega$$

$$R_i = (\beta + 1) [r_e + (3.3 \parallel 1)]$$

$$= \underline{\underline{80.0 \text{ K}\Omega}}$$

$$\frac{V_o}{V_s} = \frac{V_b}{V_s} \cdot \frac{V_o}{V_b} = \frac{R_i}{R_s + R_i} \cdot \frac{(3.3 \parallel 1)}{r_e + (3.3 \parallel 1)}$$

Thus,

$$\frac{V_o}{V_s} = \frac{80}{100 + 80} \times \frac{(3.3 \parallel 1)}{0.025 + (3.3 \parallel 1)}$$

$$= \underline{\underline{0.430 \text{ V/V}}}$$

$$\frac{I_o}{I_i} = \frac{V_o / R_L}{V_s / (R_s + R_i)}$$

$$= \frac{V_o}{V_s} \cdot \frac{(R_s + R_i)}{R_L}$$

$$= 0.43 \times \frac{(100 + 80)}{1}$$

$$= \underline{\underline{77.4 \text{ A/A}}}$$

$$R_{out} = 3.3 \parallel \left[r_e + \frac{100}{\beta + 1} \right]$$

$$= 3.3 \parallel \left[0.025 + \frac{100}{101} \right]$$

$$= \underline{\underline{0.776 \text{ K}\Omega}}$$

5.145

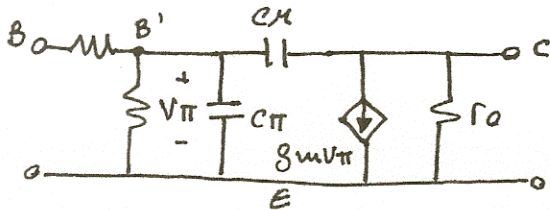
Refer to Fig 5.63(a)

$$R_o = r_o \parallel [r_e + 10 \text{ K} / (\beta + 1)]$$

CONT.

$$\begin{aligned}
 (e) \frac{V_o}{V_s} &= \frac{V_{b1}}{V_s} \cdot \frac{V_{e1}}{V_{b1}} \cdot \frac{V_o}{V_{e1}} \\
 &= 0.833 \times 0.997 \times 0.995 \\
 &= \underline{\underline{0.826 \text{ V/V}}}
 \end{aligned}$$

5.149



$$r_x = 100 \Omega$$

$$g_m = \frac{I_C}{V_T} = \frac{0.5 \text{ mA}}{25 \text{ mV}} = \underline{\underline{20 \text{ mA/V}}}$$

$$r_\pi = \frac{\beta_0}{g_m} = \frac{100}{20} = \underline{\underline{5 \text{ k}\Omega}}$$

$$R_o = \frac{V_A}{I_C} = \frac{50 \text{ V}}{0.5 \text{ mA}} = \underline{\underline{100 \text{ k}\Omega}}$$

$$C_\mu = \frac{C_{K0}}{\left(1 + \frac{V_{CE}}{V_{0c}}\right)^{0.5}} = \frac{30}{\left(1 + \frac{2}{0.75}\right)^{0.5}} = \underline{\underline{15.7 \text{ fF}}}$$

$$C_{je} \approx 2C_{je0} = 2 \times 20 = 40 \text{ fF}$$

$$C_{de} = r_F g_m = 30 \times 10^{-12} \times 20 \times 10^3 = 600 \text{ fF}$$

$$C_\pi = C_{je} + C_{de} = \underline{\underline{0.640 \text{ pF}}}$$

$$\begin{aligned}
 f_T &= \frac{g_m}{2\pi(C_\pi + C_\mu)} = \frac{20 \times 10^{-3}}{2\pi(0.64 + 0.016) \times 10^{-12}} \\
 &= \underline{\underline{4.85 \text{ GHz}}}
 \end{aligned}$$

5.150

$$|h_{fe}| \approx f_T / f$$

• At $I_C = 0.2 \text{ mA}$, $|h_{fe}| = 2.5$
at $f = 500 \text{ MHz}$, thus:

$$f_T = 2.5 \times 500 = \underline{\underline{1.25 \text{ GHz}}}$$

• At $I_C = 1.0 \text{ mA}$, $|h_{fe}| = 11.6$
at $f = 500 \text{ MHz}$, thus:
 $f_T = 11.6 \times 500 = \underline{\underline{5.8 \text{ GHz}}}$

$$f_T = \frac{g_m}{2\pi(C_\pi + C_\mu)}$$

$$C_\pi + C_\mu = \frac{g_m}{2\pi f_T} \rightarrow C_\pi = \frac{g_m}{2\pi f_T} - C_\mu$$

$$\begin{aligned}
 C_\pi (I_C = 0.2 \text{ mA}) &= \frac{8 \times 10^{-3} - 0.05 \times 10^{-12}}{2\pi \times 1.25 \times 10^9} \\
 &= \underline{\underline{0.9686 \text{ pF}}}
 \end{aligned}$$

$$\begin{aligned}
 C_\pi (I_C = 1.0 \text{ mA}) &= \frac{40 \times 10^{-3} - 0.05 \times 10^{-12}}{2\pi \times 5.8 \times 10^9} \\
 &= \underline{\underline{1.0476 \text{ pF}}}
 \end{aligned}$$

Since $C_\pi = C_{je} + r_F g_m$,
 $C_{je} + 8 \times 10^{-3} r_F = 0.9686 \times 10^{-12}$ (1)

$C_{je} + 40 \times 10^{-3} r_F = 1.0476 \times 10^{-12}$ (2)

Solving Eqs. (1) and (2)

together yields,

$$C_{je} = \underline{\underline{0.95 \text{ pF}}}, \quad r_F = \underline{\underline{247 \text{ ps}}}$$

5.151

$$\begin{aligned}
 f_T &= \frac{g_m}{2\pi(C_\pi + C_\mu)} \\
 &= \frac{80 \times 10^{-3}}{2\pi(10 + 1) \times 10^{-12}} \\
 &= \underline{\underline{4.24 \text{ GHz}}}
 \end{aligned}$$

$$\begin{aligned}
 f_\beta &= f_T / \beta_0 = (4.24 / 150) \times 10^9 \\
 &= \underline{\underline{28.26 \text{ MHz}}}
 \end{aligned}$$

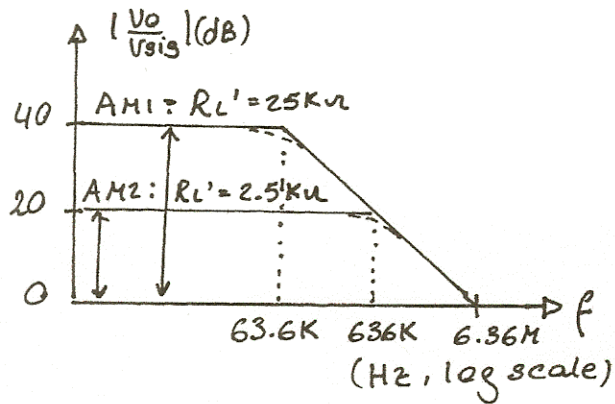
5.152

At $I_C = 2 \text{ mA}$ the diffusion part of C_π is: $10^{-2} = 8 \text{ pF}$

CONT.

$$f_H = \frac{1}{2\pi \times 10^{-12} \times 100 \times 2.5 \cdot 10^3}$$

$$f_H = \underline{\underline{636 \text{ KHz}}}$$



$$GP = 6.36 \times 10^6 = AM \times f_H$$

when $AM = 1 \Rightarrow f_H = \underline{\underline{6.36 \cdot 10^6 \text{ Hz}}}$

$$R_L' = \frac{1}{2\pi (6.36 \times 10^6) \underset{1 \times 10^{-12}}{C_H} \times \underset{100}{\beta}}$$

$$R_L' = \underline{\underline{250\Omega}}$$

5.159

Refer to Fig. P5.159

$$R_{in} = R_1 \parallel R_2 \parallel (1 + \beta r_{\pi})$$

where $R_1 = 33\text{K}\Omega$, $R_2 = 22\text{K}\Omega$

Next $\rightarrow$

CONT.

$$\begin{aligned}
 r_x &= 50 \text{ and,} \\
 r_{\pi} &= \frac{\beta_0}{g_m} = \frac{120}{0.3 \times 40} = \frac{120}{12} = 10 \text{ k}\Omega \\
 R_{in} &= 33 \parallel 22 \parallel 10.05 = \underline{\underline{5.7 \text{ k}\Omega}} \\
 A_M &= -\frac{R_{in}}{R_{in} + R_s} \cdot \frac{r_{\pi}}{r_{\pi} + r_x} \cdot g_m (R_c \parallel R_L \parallel r_o) \\
 &= -\frac{5.7}{5.7 + 5} \cdot \frac{10}{10 + 0.05} \cdot 12 (4.7 \parallel 5.6 \parallel 300) \\
 &= \underline{\underline{-16.11 \text{ V/V}}}
 \end{aligned}$$

$$\begin{aligned}
 R'_{sig} &= r_{\pi} \parallel [r_x + (R_1 \parallel R_2 \parallel R_{sig})] \\
 &= 10 \text{ k}\Omega \parallel [50 + (33 \parallel 22 \parallel 5) \text{ k}\Omega] \\
 &= \underline{\underline{2.69 \text{ k}\Omega}}
 \end{aligned}$$

$$\begin{aligned}
 R'_L &= r_o \parallel R_c \parallel R_L = 300 \parallel 4.7 \parallel 5.6 (\text{k}\Omega) \\
 &= 2.53 \text{ k}\Omega
 \end{aligned}$$

$$\begin{aligned}
 C_{\pi} + C_{\mu} &= \frac{g_m}{2\pi \cdot f_T} = \frac{12 \cdot 10^{-3}}{2\pi \times 700 \cdot 10^6} \\
 &= 2.73 \text{ pF}
 \end{aligned}$$

$$\begin{aligned}
 C_{\pi} &= (2.73 - 1) \text{ pF} \\
 &= 1.73 \text{ pF}
 \end{aligned}$$

$$\begin{aligned}
 C_{in} &= C_{\pi} + C_{\mu} (1 + g_m R'_L) \\
 &= 1.73 \text{ p} + 1 \text{ p} (1 + 12 \times 2.53) \\
 &= 33 \text{ pF}
 \end{aligned}$$

$$\begin{aligned}
 f_H &= 1 / (2\pi C_{in} R'_{sig}) \\
 &= 1 / (2\pi \times 33 \cdot 10^{-12} \times 2.69 \cdot 10^3) \\
 &= \underline{\underline{1.79 \text{ MHz}}}
 \end{aligned}$$

5.160

$$\begin{aligned}
 R_{in} &= R_1 \parallel R_2 \parallel r_{\pi} \\
 \text{where } r_{\pi} &= \frac{\beta}{g_m} \text{ and } g_m = \frac{I_C}{V_T} \\
 g_m &= \frac{0.8}{0.025} = 32 \text{ mA/V}
 \end{aligned}$$

$$r_{\pi} = \frac{200}{32} = 6.25 \text{ k}\Omega$$

$$R_{in} = 68 \parallel 27 \parallel 6.25 = 4.72 \text{ k}\Omega$$

$$R'_L = R_c \parallel R_L = 4.7 \parallel 10 = 3.2 \text{ k}\Omega$$

$$\begin{aligned}
 A_M &= \frac{R_{in}}{R_s + R_{in}} \times -g_m R'_L \\
 &= \frac{-4.72}{10 + 4.72} \times 32 \times 3.2 \\
 &= \underline{\underline{-32.8 \text{ V/V}}}
 \end{aligned}$$

$$\begin{aligned}
 C_T &= C_{\pi} + C_{\mu} (1 + g_m R'_L) \\
 \text{where } C_{\pi} + C_{\mu} &= \frac{g_m}{2\pi f_T} = \frac{32 \times 10^{-3}}{2\pi \times 10^9} \\
 &= 5.1 \text{ pF}
 \end{aligned}$$

$$C_{\pi} = 5.1 - 0.8 = 4.3 \text{ pF}$$

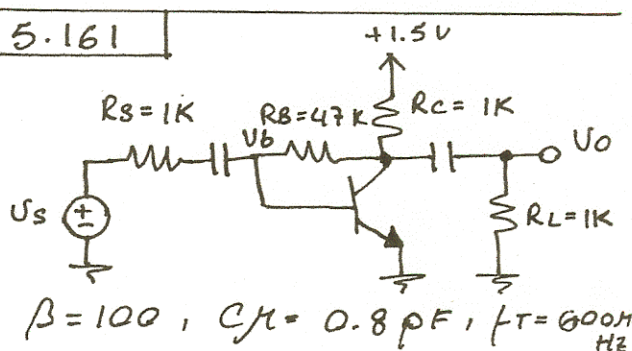
$$\begin{aligned}
 C_T &= 4.3 + 0.8 (1 + 32 \times 3.2) \\
 &= 87 \text{ pF}
 \end{aligned}$$

The resistance seen by C_T is R_T ,

$$\begin{aligned}
 R_T &= r_{\pi} \parallel R_1 \parallel R_2 \parallel R_s \\
 &= 6.25 \parallel 68 \parallel 27 \parallel 10 = 3.2 \text{ k}\Omega
 \end{aligned}$$

Thus

$$\begin{aligned}
 f_H &\approx \frac{1}{2\pi C_T R_T} \\
 &= \frac{1}{2\pi \times 87 \times 10^{-12} \times 3.2 \times 10^3} \\
 &= \underline{\underline{572 \text{ kHz}}}
 \end{aligned}$$



CONT.