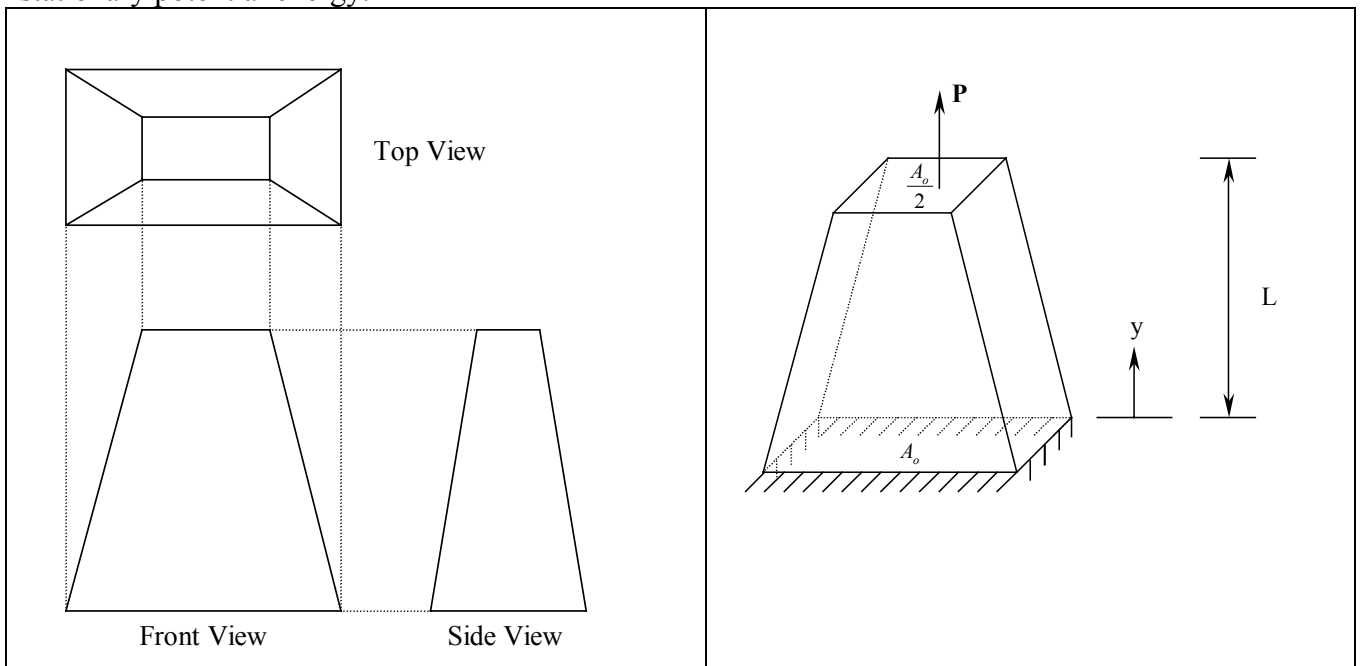


### Principle of Stationery Potential Energy

Among all admissible displaced configurations of a conservative system those that satisfy equations of equilibrium make the potential energy stationery with respect to small admissible variations of displacement. If the stationery condition is a relative minimum, the equilibrium state is stable.

#### Example:

A tapered bar as shown in the figure is subject to an axial load 'P'. The area of the tapered bar varies linearly from  $y = 0$  to  $y = L$ , from,  $A_o$  to  $\frac{A_o}{2}$ . Assuming an admissible displacement of  $v(y) = b_0 y + c_0 y^2$ , find the displacement of  $y = L$  using the principle of stationary potential energy.



Assume an expression for the area 'A' as

$$A = my + c$$

then

$$A_o = m(0) + c$$

$$\frac{A_o}{2} = m(L) + c$$

$$c = A_o$$

$$m = -\frac{A_o}{2L}$$

$$A = -\frac{A_o}{2L}y + A_o$$

$$\begin{aligned}
&= \frac{A_o}{2L}(2L - y) \\
U &= \int_V \frac{1}{2} \sigma_y \epsilon_y dV \\
&= \int_V \frac{1}{2} E \epsilon_y \epsilon_y dV \\
&= \int_V \frac{1}{2} E \left( \frac{dv}{dy} \right) \left( \frac{dv}{dy} \right) dV \\
&= \int_V \frac{1}{2} E \left( \frac{dv}{dy} \right)^2 dV \\
&= \int_{o-V}^V \frac{1}{2} E \left( \frac{dv}{dy} \right)^2 A dy
\end{aligned}$$

$$W = Pv_L$$

$$\Pi = U - W$$

$$= \int_0^L \frac{1}{2} E \left( \frac{dv}{dy} \right)^2 A dy - Pv_L$$

Assuming

$$v = b_o y + c_o y^2$$

$$\frac{dv}{dy} = b_o + 2c_o y$$

$$= \left[ \int_0^L \frac{1}{2} E (b_o + 2c_o y)^2 \left( \frac{A_o}{2L} (2L - y) \right) dy \right] - P(b_o L + c_o L^2)$$

$$= \frac{EA_o L}{24} (10L^2 c_o^2 + 16b_o c_o L + 9b_o^2) - P(b_o L + c_o L^2)$$

$$\frac{\partial \Pi}{\partial b_o} = 0$$

gives

$$8EA_o c_o L + 9EA_o b_o - 12P = 0 \dots \dots \dots (1)$$

$$\frac{\partial \Pi}{\partial c_o} = 0$$

gives

$$5EA_o c_o L + 4EA_o b_o - 6P = 0 \dots \dots \dots (2)$$

From (1) and (2), we get

$$b_o = \frac{12}{13} \frac{P}{EA_o}$$

$$c_o = \frac{6}{13} \frac{P}{EA_o L}$$

Hence

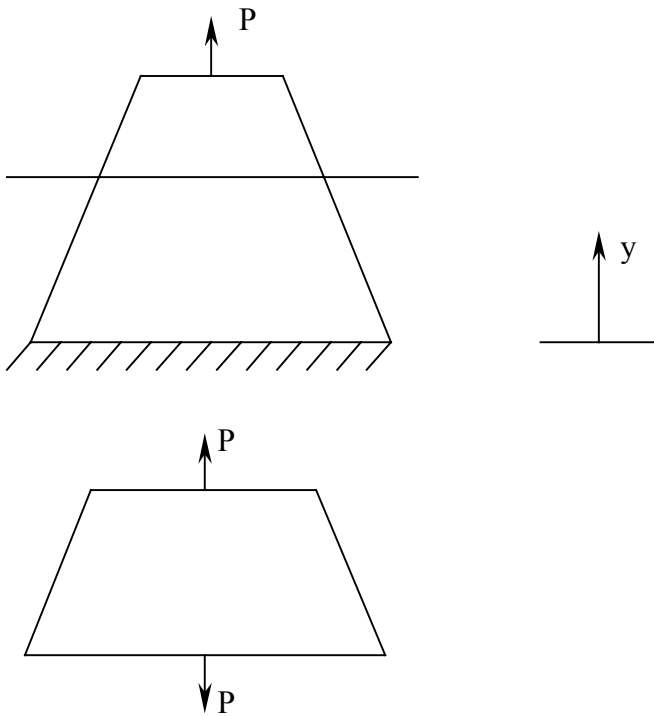
$$v = \frac{12}{13} \frac{P}{EA_o} y + \frac{6}{13} \frac{P}{EA_o L} y^2$$

$$v_L = \frac{12}{13} \frac{P}{EA_o} L + \frac{6}{13} \frac{P}{EA_o L} L^2$$

$$= \frac{18}{13} \frac{PL}{EA_o}$$

$$= 1.38462 \frac{PL}{EA_o}$$

**Exact Solution:**



$$\epsilon_y = \frac{\sigma_y}{E}$$

$$= \frac{P}{AE}$$

$$= \frac{P}{\frac{A_o}{2L} (2L-x) E}$$

$$\frac{dv}{dy} = \frac{2PL}{A_o(2L-x)E}$$

$$v_y - v_{y=0} = \int_0^y \frac{2PL}{A_o(2L-y')E} dy'$$

$$= \frac{2PL}{A_oE} \ln\left(\frac{2L}{2L-y}\right)$$

$$v_y = \frac{2PL}{A_oE} \ln\left(\frac{2L}{2L-y}\right)$$

$$v_L = \frac{PL}{AE} (2\ln 2)$$

$$= 1.38629 \frac{PL}{EA_o}$$

The absolute relative true error is

$$|\epsilon_t| = \left| \frac{\text{Exact Value} - \text{Aprox Value}}{\text{Exact value}} \right| \times 100$$

$$|\epsilon_t| = \left| \frac{\frac{PL}{A_oE} (2\ln 2) - \frac{18}{13} \frac{PL}{A_oE}}{\frac{PL}{A_oE} (2\ln 2)} \right| \times 100$$

$$= 0.11\%$$