

# EML 4230 Introduction to Composite Materials

## Chapter 4 Macromechanical Analysis of a Laminate **Hygrothermal Loads**

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Courtesy of the Textbook  
[Mechanics of Composite Materials by Kaw](#)

# Mechanical Strains

$$\begin{bmatrix} \varepsilon_x^M \\ \varepsilon_y^M \\ \gamma_{xy}^M \end{bmatrix}_k = \begin{bmatrix} \varepsilon_x \\ \varepsilon_y \\ \gamma_{xy} \end{bmatrix} - \begin{bmatrix} \varepsilon_x^T \\ \varepsilon_y^T \\ \gamma_{xy}^T \end{bmatrix}_k = \begin{bmatrix} \varepsilon_x \\ \varepsilon_y \\ \gamma_{xy} \end{bmatrix} - \begin{bmatrix} \alpha_x \Delta T \\ \alpha_y \Delta T \\ \alpha_{xy} \Delta T \end{bmatrix}_k$$

# Hygrothermal Stresses

$$\begin{bmatrix} \sigma_x^T \\ \sigma_y^T \\ \gamma_{xy}^T \end{bmatrix}_k = \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{16} \\ \bar{Q}_{12} & \bar{Q}_{22} & \bar{Q}_{26} \\ \bar{Q}_{16} & \bar{Q}_{26} & \bar{Q}_{66} \end{bmatrix}_k \begin{bmatrix} \varepsilon_x^M \\ \varepsilon_y^M \\ \gamma_{xy}^M \end{bmatrix}_k$$

# Zero resultant stresses

$$\int_{-h/2}^{h/2} \begin{bmatrix} \sigma_x^T \\ \sigma_y^T \\ \tau_{xy}^T \end{bmatrix} dz = 0$$

$$\sum_{k=1}^n \int_{h_{k-1}}^{h_k} \begin{bmatrix} \sigma_x^T \\ \sigma_y^T \\ \tau_{xy}^T \end{bmatrix}_k dz = 0$$

# Zero resultant stresses

$$\sum_{k=1}^n \int_{h_{k-1}}^{h_k} \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{16} \\ \bar{Q}_{12} & \bar{Q}_{22} & \bar{Q}_{26} \\ \bar{Q}_{16} & \bar{Q}_{26} & \bar{Q}_{66} \end{bmatrix}_k \begin{bmatrix} \varepsilon_x^M \\ \varepsilon_y^M \\ \gamma_{xy}^M \end{bmatrix}_k dz = 0$$

# Deriving final formula

$$\sum_{k=1}^n \int_{h_{k-1}}^{h_k} \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{16} \\ \bar{Q}_{12} & \bar{Q}_{22} & \bar{Q}_{26} \\ \bar{Q}_{16} & \bar{Q}_{26} & \bar{Q}_{66} \end{bmatrix}_k \begin{pmatrix} \varepsilon_x \\ \varepsilon_y \\ \gamma_{xy}^0 \end{pmatrix}_k - \begin{pmatrix} \varepsilon_x^T \\ \varepsilon_y^T \\ \gamma_{xy}^T \end{pmatrix}_k \right) dz = 0$$

$$\sum_{k=1}^n \int_{h_{k-1}}^{h_k} \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{16} \\ \bar{Q}_{12} & \bar{Q}_{22} & \bar{Q}_{26} \\ \bar{Q}_{16} & \bar{Q}_{26} & \bar{Q}_{66} \end{bmatrix}_k \begin{pmatrix} \varepsilon_x^0 \\ \varepsilon_y^0 \\ \gamma_{xy}^0 \end{pmatrix} + z \begin{pmatrix} \kappa_x \\ \kappa_y \\ \kappa_{xy} \end{pmatrix} - \begin{pmatrix} \varepsilon_x^T \\ \varepsilon_y^T \\ \gamma_{xy}^T \end{pmatrix}_k \right) dz = 0$$

# Deriving final formula

$$\sum_{k=1}^n \int_{h_{k-1}}^{h_k} \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{16} \\ \bar{Q}_{12} & \bar{Q}_{22} & \bar{Q}_{26} \\ \bar{Q}_{16} & \bar{Q}_{26} & \bar{Q}_{66} \end{bmatrix}_k \begin{Bmatrix} \varepsilon_x^0 \\ \varepsilon_y^0 \\ \gamma_{xy}^0 \end{Bmatrix} + z \begin{Bmatrix} \kappa_x \\ \kappa_y \\ \kappa_{xy} \end{Bmatrix} dz =$$

$$\sum_{k=1}^n \int_{h_{k-1}}^{h_k} \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{16} \\ \bar{Q}_{12} & \bar{Q}_{22} & \bar{Q}_{26} \\ \bar{Q}_{16} & \bar{Q}_{26} & \bar{Q}_{66} \end{bmatrix}_k \begin{Bmatrix} \varepsilon_x^T \\ \varepsilon_y^T \\ \gamma_{xy}^T \end{Bmatrix} dz$$

# Deriving final formula

$$\sum_{k=1}^n \int_{h_{k-1}}^{h_k} \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{16} \\ \bar{Q}_{12} & \bar{Q}_{22} & \bar{Q}_{26} \\ \bar{Q}_{16} & \bar{Q}_{26} & \bar{Q}_{66} \end{bmatrix}_k \begin{Bmatrix} \varepsilon_x^0 \\ \varepsilon_y^0 \\ \gamma_{xy}^0 \end{Bmatrix} + z \begin{Bmatrix} \boldsymbol{\kappa}_x \\ \boldsymbol{\kappa}_y \\ \boldsymbol{\kappa}_{xy} \end{Bmatrix} dz =$$

$$\sum_{k=1}^n \int_{h_{k-1}}^{h_k} \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{16} \\ \bar{Q}_{12} & \bar{Q}_{22} & \bar{Q}_{26} \\ \bar{Q}_{16} & \bar{Q}_{26} & \bar{Q}_{66} \end{bmatrix}_k \begin{bmatrix} \alpha_x \\ \alpha_y \\ \alpha_{xy} \end{bmatrix}_k \Delta T dz$$

# Deriving final formula

$$\begin{bmatrix} A_{11} & A_{12} & A_{16} \\ A_{12} & A_{22} & A_{26} \\ A_{16} & A_{26} & A_{66} \end{bmatrix} \begin{bmatrix} \varepsilon_x^o \\ \varepsilon_y^o \\ \gamma_{xy}^o \end{bmatrix} + \begin{bmatrix} B_{11} & B_{12} & B_{16} \\ B_{12} & B_{22} & B_{26} \\ B_{16} & B_{26} & B_{66} \end{bmatrix} \begin{bmatrix} \kappa_x \\ \kappa_y \\ \kappa_{xy} \end{bmatrix} = \begin{bmatrix} N_x^T \\ N_y^T \\ N_{xy}^T \end{bmatrix}$$

$$[N^T] = \begin{bmatrix} N_x^T \\ N_y^T \\ N_{xy}^T \end{bmatrix} = \Delta T \sum_{k=1}^n \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{16} \\ \bar{Q}_{12} & \bar{Q}_{22} & \bar{Q}_{26} \\ \bar{Q}_{16} & \bar{Q}_{26} & \bar{Q}_{66} \end{bmatrix}_k \begin{bmatrix} \alpha_x \\ \alpha_y \\ \alpha_{xy} \end{bmatrix}_k (h_k - h_{k-1})$$

# Other three equations – from zero resultant moments

$$\begin{bmatrix} B_{11} & B_{12} & B_{16} \\ B_{12} & B_{22} & B_{26} \\ B_{16} & B_{26} & B_{66} \end{bmatrix} \begin{bmatrix} \varepsilon_x^o \\ \varepsilon_y^o \\ \gamma_{xy}^o \end{bmatrix} + \begin{bmatrix} D_{11} & D_{12} & D_{16} \\ D_{12} & D_{22} & D_{26} \\ D_{16} & D_{26} & D_{66} \end{bmatrix} \begin{bmatrix} \kappa_x \\ \kappa_y \\ \kappa_{xy} \end{bmatrix} = \begin{bmatrix} M_x^T \\ M_y^T \\ M_{xy}^T \end{bmatrix}$$

$$[M^T] = \begin{bmatrix} M_x^T \\ M_y^T \\ M_{xy}^T \end{bmatrix} = \frac{1}{2} \Delta T \sum_{k=1}^n \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{16} \\ \bar{Q}_{12} & \bar{Q}_{22} & \bar{Q}_{26} \\ \bar{Q}_{16} & \bar{Q}_{26} & \bar{Q}_{66} \end{bmatrix}_k \begin{bmatrix} \alpha_x \\ \alpha_y \\ \alpha_{xy} \end{bmatrix}_k (h_k^2 - h_{k-1}^2)$$

# Final formula

$$\begin{bmatrix} N^T \\ M^T \end{bmatrix} = \begin{bmatrix} A/B \\ B/D \end{bmatrix} \begin{bmatrix} \varepsilon^0 \\ \kappa \end{bmatrix}$$

$$[N^T] = \begin{bmatrix} N_x^T \\ N_y^T \\ N_{xy}^T \end{bmatrix} = \Delta T \sum_{k=1}^n \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{16} \\ \bar{Q}_{12} & \bar{Q}_{22} & \bar{Q}_{26} \\ \bar{Q}_{16} & \bar{Q}_{26} & \bar{Q}_{66} \end{bmatrix}_k \begin{bmatrix} \alpha_x \\ \alpha_y \\ \alpha_{xy} \end{bmatrix}_k (h_k - h_{k-1})$$

$$[M^T] = \begin{bmatrix} M_x^T \\ M_y^T \\ M_{xy}^T \end{bmatrix} = \frac{1}{2} \Delta T \sum_{k=1}^n \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{16} \\ \bar{Q}_{12} & \bar{Q}_{22} & \bar{Q}_{26} \\ \bar{Q}_{16} & \bar{Q}_{26} & \bar{Q}_{66} \end{bmatrix}_k \begin{bmatrix} \alpha_x \\ \alpha_y \\ \alpha_{xy} \end{bmatrix}_k (h_k^2 - h_{k-1}^2)$$

# Final formula

$$\begin{bmatrix} \varepsilon_x^M \\ \varepsilon_y^M \\ \gamma_{xy}^M \end{bmatrix}_k = \begin{bmatrix} \varepsilon_x \\ \varepsilon_y \\ \gamma_{xy} \end{bmatrix}_k - \begin{bmatrix} \varepsilon_x^T \\ \varepsilon_y^T \\ \gamma_{xy}^T \end{bmatrix}_k$$
$$= \begin{bmatrix} \varepsilon_x \\ \varepsilon_y \\ \gamma_{xy} \end{bmatrix}_k - \begin{bmatrix} \alpha_x \Delta T \\ \alpha_y \Delta T \\ \alpha_{xy} \Delta T \end{bmatrix}_k$$

# Example 4.5

Calculate the residual stresses at the bottom surface of the  $90^\circ$  ply in a two ply [0/90] Graphite/Epoxy laminate subjected to a temperature change of  $-75^\circ\text{C}$ . Use the unidirectional properties of Graphite/Epoxy lamina from Table 2.1. Each lamina is  $5 \text{ mm}$  thick.

## Example 4.5

$$\begin{bmatrix} \alpha_1 \\ \alpha_2 \\ \alpha_{12} \end{bmatrix} = \begin{bmatrix} 0.200 \times 10^{-7} \\ 0.225 \times 10^{-4} \\ 0 \end{bmatrix} m/m /{}^o C$$

$$\begin{bmatrix} \alpha_x \\ \alpha_y \\ \alpha_{xy} \end{bmatrix}_{0^o} = \begin{bmatrix} 0.200 \times 10^{-7} \\ 0.225 \times 10^{-4} \\ 0 \end{bmatrix} m/m /{}^o C$$

$$\begin{bmatrix} \alpha_x \\ \alpha_y \\ \alpha_{xy} \end{bmatrix}_{90^o} = \begin{bmatrix} 0.225 \times 10^{-4} \\ 0.200 \times 10^{-7} \\ 0 \end{bmatrix} m/m /{}^o C$$

## Example 4.5

$$[\bar{Q}]_0 = \begin{bmatrix} 181.8 & 2.897 & 0 \\ 2.897 & 10.35 & 0 \\ 0 & 0 & 7.17 \end{bmatrix} GPa$$

$$[\bar{Q}]_{90} = \begin{bmatrix} 10.35 & 2.897 & 0 \\ 2.897 & 181.8 & 0 \\ 0 & 0 & 7.17 \end{bmatrix} GPa$$

# Example 4.5

$$\begin{bmatrix} N_x^T \\ N_y^T \\ N_{xy}^T \end{bmatrix} = + (-75) \begin{bmatrix} 181.8 & 2.897 & 0 \\ 2.897 & 10.35 & 0 \\ 0 & 0 & 7.17 \end{bmatrix} (10^9) \begin{bmatrix} 0.200 (10^{-7}) \\ 0.225 (10^{-4}) \\ 0 \end{bmatrix} [0.000 - (-0.005)]$$
$$+ (-75) \begin{bmatrix} 10.35 & 2.897 & 0 \\ 2.897 & 181.8 & 0 \\ 0 & 0 & 7.17 \end{bmatrix} (10^9) \begin{bmatrix} 0.225 (10^4) \\ 0.200 (10^7) \\ 0 \end{bmatrix} [0.005 - 0.000]$$
$$= \begin{bmatrix} -1.131 \times 10^5 \\ -1.131 \times 10^5 \\ 0 \end{bmatrix} Pa \cdot m.$$

# Example 4.5

$$\begin{bmatrix} M_x^T \\ M_y^T \\ M_{xy}^T \end{bmatrix} = \frac{1}{2} (-75) \begin{bmatrix} 181.8 & 2.897 & 0 \\ 2.897 & 10.35 & 0 \\ 0 & 0 & 7.17 \end{bmatrix} (10^9) \begin{bmatrix} 0.200 \times 10^{-7} \\ 0.225 \times 10^{-4} \\ 0 \end{bmatrix} [(0.000)^2 - (-0.005)^2]$$

$$+ \frac{1}{2} (-75) \begin{bmatrix} 10.35 & 2.897 & 0 \\ 2.897 & 10.35 & 0 \\ 0 & 0 & 7.17 \end{bmatrix} (10^9) \begin{bmatrix} 0.225 \times 10^{-4} \\ 0.200 \times 10^{-7} \\ 0 \end{bmatrix} [(0.005)^2 - (0.000)^2]$$

$$= \begin{bmatrix} -1.538 \times 10^2 \\ 1.538 \times 10^2 \\ 0 \end{bmatrix} Pa\ m$$

# Example 4-5

$$[A] = \begin{bmatrix} 9.608 \times 10^8 & 2.897 \times 10^7 & 0 \\ 2.897 \times 10^7 & 9.608 \times 10^8 & 0 \\ 0 & 0 & 7.170 \times 10^7 \end{bmatrix} Pa \cdot m$$

$$[B] = \begin{bmatrix} -2.143 \times 10^6 & 0 & 0 \\ 0 & 2.143 \times 10^6 & 0 \\ 0 & 0 & 0 \end{bmatrix} Pa \cdot m^2$$

$$[D] = \begin{bmatrix} 8.007 \times 10^3 & 2.414 \times 10^2 & 0 \\ 2.414 \times 10^2 & 8.007 \times 10^3 & 0 \\ 0 & 0 & 5.975 \times 10^2 \end{bmatrix} Pa \cdot m^3$$

# Example 4.5

$$\begin{bmatrix} -1.131 \times 10^5 \\ -1.131 \times 10^5 \\ 0 \\ -1.538 \times 10^2 \\ 1.538 \times 10^2 \\ 0 \end{bmatrix} = \begin{bmatrix} 9.608 \times 10^8 & 2.897 \times 10^7 & 0 & -2.143 \times 10^6 & 0 & 0 \\ 2.897 \times 10^7 & 9.608 \times 10^8 & 0 & 0 & 2.143 \times 10^6 & 0 \\ 0 & 0 & 7.170 \times 10^7 & 0 & 0 & 0 \\ -2.143 \times 10^6 & 0 & 0 & 8.007 \times 10^3 & 2.414 \times 10^2 & 0 \\ 0 & 2.143 \times 10^6 & 0 & 2.414 \times 10^2 & 8.007 \times 10^3 & 0 \\ 0 & 0 & 0 & 0 & 0 & 5.975 \times 10^2 \end{bmatrix} \begin{bmatrix} \varepsilon_x^0 \\ \varepsilon_y^0 \\ \gamma_{xy}^0 \\ \kappa_x \\ \kappa_y \\ \kappa_{xy} \end{bmatrix}$$

$$\begin{bmatrix} \varepsilon_x^0 \\ \varepsilon_y^0 \\ \gamma_{xy}^0 \\ \kappa_x \\ \kappa_y \\ \kappa_{xy} \end{bmatrix} = \begin{bmatrix} -3.907 \times 10^{-4} \\ -3.907 \times 10^{-4} \\ 0 \\ \frac{-1.276 \times 10^{-1}}{1.276 \times 10^{-1}} \\ 1.276 \times 10^{-1} \\ 0 \end{bmatrix} \begin{array}{l} m/m \\ 1/m \end{array}$$

$$\begin{bmatrix} N^T \\ M^T \end{bmatrix} = \begin{bmatrix} A & B \\ B & D \end{bmatrix} \begin{bmatrix} \varepsilon^0 \\ \kappa \end{bmatrix}$$

## Example 4.5

$$\begin{bmatrix} \varepsilon_x \\ \varepsilon_y \\ \gamma_{xy} \end{bmatrix}_{90^\circ} = \begin{bmatrix} -3.907 \times 10^{-4} \\ -3.907 \times 10^{-4} \\ 0 \end{bmatrix} + (0.005) \begin{bmatrix} -1.276 \times 10^{-1} \\ 1.276 \times 10^{-1} \\ 0 \end{bmatrix}$$

$$= \begin{bmatrix} -1.029 \times 10^{-3} \\ 2.475 \times 10^{-4} \\ 0 \end{bmatrix} m/m$$

# Example 4.5

$$\begin{bmatrix} \varepsilon_x^T \\ \varepsilon_y^T \\ \gamma_{xy}^T \end{bmatrix} = \begin{bmatrix} 0.225 \times 10^{-4} \\ 0.200 \times 10^{-7} \\ 0 \end{bmatrix} (-75)$$

$$= \begin{bmatrix} -0.16875 \times 10^{-2} \\ -0.15000 \times 10^{-5} \\ 0 \end{bmatrix} m/m$$

# Example 4.5

$$\begin{bmatrix} \varepsilon_x^M \\ \varepsilon_y^M \\ \gamma_{xy}^M \end{bmatrix} = \begin{bmatrix} -1.029 \times 10^{-3} \\ 2.475 \times 10^{-4} \\ 0 \end{bmatrix} - \begin{bmatrix} -0.16875 \times 10^{-2} \\ -0.1500 \times 10^{-5} \\ 0 \end{bmatrix} = \begin{bmatrix} 0.6585 \times 10^{-3} \\ 0.2490 \times 10^{-3} \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} \sigma_x \\ \sigma_y \\ \tau_{xy} \end{bmatrix}_{90^0} = \begin{bmatrix} 10.35 & 2.897 & 0 \\ 2.897 & 181.8 & 0 \\ 0 & 0 & 7.17 \end{bmatrix} (10^9) \begin{bmatrix} 0.6585 \times 10^{-3} \\ 0.2490 \times 10^{-3} \\ 0 \end{bmatrix} = \begin{bmatrix} 7.535 \times 10^6 \\ 4.718 \times 10^7 \\ 0 \end{bmatrix} Pa.$$

# Example 4.5

Global Strains for Example 4.3

Ply #	Position	$\varepsilon_x$	$\varepsilon_y$	$\gamma_{xy}$
1 ( $0^0$ )	Top	$2.475 \times 10^{-4}$	$-1.029 \times 10^{-3}$	0.0
	Middle	$-7.160 \times 10^{-5}$	$-7.098 \times 10^{-4}$	0.0
	Bottom	$-3.907 \times 10^{-4}$	$-3.907 \times 10^{-4}$	0.0
2 ( $90^0$ )	Top	$-3.907 \times 10^{-4}$	$-3.907 \times 10^{-4}$	0.0
	Middle	$-7.098 \times 10^{-4}$	$-7.160 \times 10^{-5}$	0.0
	Bottom	$-1.029 \times 10^{-3}$	$2.475 \times 10^{-4}$	0.0

# Example 4-5

Global Stresses for Example 4-3

Ply #	Position	$\sigma_y$	$\sigma_x$	$\tau_{xy}$
1( $0^0$ )	Top	$4.718 \times 10^7$	$7.535 \times 10^6$	0.0
	Middle	$-9.912 \times 10^6$	$9.912 \times 10^6$	0.0
	Bottom	$-6.701 \times 10^7$	$1.229 \times 10^7$	0.0
2( $90^0$ )	Top	$1.229 \times 10^7$	$-6.701 \times 10^7$	0.0
	Middle	$9.912 \times 10^6$	$-9.912 \times 10^6$	0.0
	Bottom	$7.535 \times 10^6$	$4.718 \times 10^7$	0.0

# Coefficients of Thermal and Moisture Expansion

To find coefficients of thermal and moisture expansion of laminates

- Symmetric laminates  $[B] = 0$
- No bending occurs under thermal hygrothermal loads
- Assuming  $\Delta T = 1$  and  $\Delta C = 0$

$$\begin{bmatrix} A_{11} & A_{12} & A_{16} \\ A_{12} & A_{22} & A_{26} \\ A_{16} & A_{26} & A_{66} \end{bmatrix} \begin{bmatrix} \varepsilon_x^0 \\ \varepsilon_y^0 \\ \gamma_{xy}^0 \end{bmatrix} + \begin{bmatrix} B_{11} & B_{12} & B_{16} \\ B_{12} & B_{22} & B_{26} \\ B_{16} & B_{26} & B_{66} \end{bmatrix} \begin{bmatrix} \kappa_x \\ \kappa_y \\ \kappa_{xy} \end{bmatrix} = \begin{bmatrix} N_x^T \\ N_y^T \\ N_{xy}^T \end{bmatrix} + \begin{bmatrix} N_x^C \\ N_y^C \\ N_{xy}^C \end{bmatrix}$$

$$\begin{bmatrix} \alpha_x \\ \alpha_y \\ \alpha_{xy} \end{bmatrix} \equiv \begin{bmatrix} \varepsilon_x^0 \\ \varepsilon_y^0 \\ \gamma_{xy}^0 \end{bmatrix}_{\Delta C=0} = \begin{bmatrix} A_{11}^* & A_{12}^* & A_{16}^* \\ A_{12}^* & A_{22}^* & A_{26}^* \\ A_{16}^* & A_{26}^* & A_{66}^* \end{bmatrix} \begin{bmatrix} N_x^T \\ N_y^T \\ N_{xy}^T \end{bmatrix}_{\Delta T=1}$$

# Coefficients of Thermal and Moisture Expansion

To find coefficients of thermal and moisture expansion of laminates

- Symmetric laminates  $[B] = 0$
- No bending occurs under thermal hygrothermal loads
- Assuming  $\Delta T = 0$  and  $\Delta C = 1$

$$\begin{bmatrix} A_{11} & A_{12} & A_{16} \\ A_{12} & A_{22} & A_{26} \\ A_{16} & A_{26} & A_{66} \end{bmatrix} \begin{bmatrix} \varepsilon_x^0 \\ \varepsilon_y^0 \\ \gamma_{xy}^0 \end{bmatrix} + \begin{bmatrix} B_{11} & B_{12} & B_{16} \\ B_{12} & B_{22} & B_{26} \\ B_{16} & B_{26} & B_{66} \end{bmatrix} \begin{bmatrix} \kappa_x \\ \kappa_y \\ \kappa_{xy} \end{bmatrix} = \begin{bmatrix} N_x^T \\ N_y^T \\ N_{xy}^T \end{bmatrix} + \begin{bmatrix} N_x^C \\ N_y^C \\ N_{xy}^C \end{bmatrix}$$

$$\begin{bmatrix} \beta_x \\ \beta_y \\ \beta_{xy} \end{bmatrix} \underset{\Delta T = 0}{\equiv} \begin{bmatrix} \varepsilon_x^0 \\ \varepsilon_y^0 \\ \gamma_{xy}^0 \end{bmatrix} = \begin{bmatrix} A_{11}^* & A_{12}^* & A_{16}^* \\ A_{12}^* & A_{22}^* & A_{26}^* \\ A_{16}^* & A_{26}^* & A_{66}^* \end{bmatrix} \begin{bmatrix} N_x^C \\ N_y^C \\ N_{xy}^C \end{bmatrix}$$

$\Delta C = I$

## Example 4.6

Find the coefficients of thermal and moisture expansion of a  $[0/\overline{90}]_s$  Graphite/Epoxy laminate. Use the properties of unidirectional Graphite/Epoxy lamina from table 2.1.

## Example 4.6

$$[A^*] = \begin{bmatrix} 5.353 \times 10^{-10} & -2.297 \times 10^{-11} & 0 \\ -2.297 \times 10^{-11} & 9.886 \times 10^{-10} & 0 \\ 0 & 0 & 9.298 \times 10^{-9} \end{bmatrix} \frac{1}{Pa \cdot m}$$

# Example 4.6

$$\begin{bmatrix} N_x^T \\ N_y^T \\ N_{xy}^T \end{bmatrix} = \Delta T \sum_{k=1}^3 \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{16} \\ \bar{Q}_{12} & \bar{Q}_{22} & \bar{Q}_{26} \\ \bar{Q}_{16} & \bar{Q}_{26} & \bar{Q}_{66} \end{bmatrix}_k \begin{bmatrix} \alpha_x \\ \alpha_y \\ \alpha_{xy} \end{bmatrix}_k (h_k - h_{k-1})$$

$$= (1) \begin{bmatrix} 181.8 & 2.897 & 0 \\ 2.897 & 10.35 & 0 \\ 0 & 0 & 7.17 \end{bmatrix} (10^9) \begin{bmatrix} 0.200 \times 10^{-7} \\ 0.225 \times 10^{-4} \\ 0 \end{bmatrix} [-0.0025 - (-0.0075)]$$

$$+ (1) \begin{bmatrix} 10.35 & 2.897 & 0 \\ 2.897 & 181.35 & 0 \\ 0 & 0 & 7.17 \end{bmatrix} (10^9) \begin{bmatrix} 0.225 \times 10^{-4} \\ 0.200 \times 10^{-7} \\ 0 \end{bmatrix} [0.0025 - (-0.0025)]$$

$$+ (1) \begin{bmatrix} 181.8 & 2.897 & 0 \\ 2.897 & 10.35 & 0 \\ 0 & 0 & 7.17 \end{bmatrix} (10^9) \begin{bmatrix} 0.200 \times 10^{-7} \\ 0.225 \times 10^{-4} \\ 0 \end{bmatrix} [0.0075 - 0.0025] = \begin{bmatrix} 1.852 \times 10^3 \\ 2.673 \times 10^3 \\ 0 \end{bmatrix} Pa \cdot m$$

## Example 4.6

$$\begin{bmatrix} \varepsilon_x^0 \\ \varepsilon_y^0 \\ \gamma_{xy}^0 \end{bmatrix} = \begin{bmatrix} 5.353 \times 10^{-10} & -2.297 \times 10^{-11} & 0 \\ -2.297 \times 10^{-11} & 9.886 \times 10^{-10} & 0 \\ 0 & 0 & 9.298 \times 10^{-9} \end{bmatrix} \begin{bmatrix} 1.852 \times 10^3 \\ 2.673 \times 10^3 \\ 0 \end{bmatrix}$$
$$= \begin{bmatrix} 9.303 \times 10^{-7} \\ 2.600 \times 10^{-6} \\ 0 \end{bmatrix} m/m.$$

$$\begin{bmatrix} \alpha_x \\ \alpha_y \\ \alpha_{xy} \end{bmatrix} \equiv \begin{bmatrix} \varepsilon_x^0 \\ \varepsilon_y^0 \\ \gamma_{xy}^0 \end{bmatrix}_{\Delta C=0} = = \begin{bmatrix} 9.303 \times 10^{-7} \\ 2.600 \times 10^{-6} \\ 0 \end{bmatrix} m/m / {}^\circ C$$
$$\qquad \qquad \qquad \Delta T = 1$$

# Example 4.6

$$\begin{bmatrix} N_x^C \\ N_y^C \\ N_{xy}^C \end{bmatrix} = \Delta C \sum_{k=1}^3 \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{16} \\ \bar{Q}_{12} & \bar{Q}_{22} & \bar{Q}_{26} \\ \bar{Q}_{16} & \bar{Q}_{26} & \bar{Q}_{66} \end{bmatrix}_k \begin{bmatrix} \beta_x \\ \beta_y \\ \beta_{xy} \end{bmatrix} (h_k - h_{k-1}) \quad \Delta C = 1 \text{ kg/kg}$$

$$= (1) \begin{bmatrix} 181.8 & 2.897 & 0 \\ 2.897 & 10.35 & 0 \\ 0 & 0 & 7.17 \end{bmatrix} (10^9) \begin{bmatrix} 0 \\ 0.6 \\ 0 \end{bmatrix} [-0.0025 - (-0.0075)]$$

$$+ (1) \begin{bmatrix} 10.35 & 2.897 & 0 \\ 2.897 & 181.35 & 0 \\ 0 & 0 & 7.17 \end{bmatrix} (10^9) \begin{bmatrix} 0.6 \\ 0 \\ 0 \end{bmatrix} [0.0025 - (-0.0025)]$$

$$+ (1) \begin{bmatrix} 181.8 & 2.897 & 0 \\ 2.897 & 10.35 & 0 \\ 0 & 0 & 7.17 \end{bmatrix} (10^9) \begin{bmatrix} 0 \\ 0.6 \\ 0 \end{bmatrix} [0.0075 - 0.0025] = \begin{bmatrix} 4.842 \times 10^7 \\ 7.077 \times 10^7 \\ 0 \end{bmatrix} Pa \cdot m$$

# Example 4.6

$$\begin{bmatrix} \varepsilon_x^0 \\ \varepsilon_y^0 \\ \gamma_{xy}^0 \end{bmatrix} = \begin{bmatrix} 5.353 \times 10^{-10} & -2.297 \times 10^{-11} & 0 \\ -2.297 \times 10^{-11} & 9.886 \times 10^{-10} & 0 \\ 0 & 0 & 9.298 \times 10^{-9} \end{bmatrix} \begin{bmatrix} 4.842 \times 10^7 \\ 7.077 \times 10^7 \\ 0 \end{bmatrix}$$
$$= \begin{bmatrix} 2.430 \times 10^{-2} \\ 6.885 \times 10^{-2} \\ 0 \end{bmatrix} m/m$$

$$\begin{bmatrix} \beta_x \\ \beta_y \\ \beta_{xy} \end{bmatrix} \equiv \begin{bmatrix} \varepsilon_x^0 \\ \varepsilon_y^0 \\ \gamma_{xy}^0 \end{bmatrix}_{\Delta C=1} = \begin{bmatrix} 2.430 \times 10^{-2} \\ 6.885 \times 10^{-2} \\ 0 \end{bmatrix} m/m / kg / kg$$
$$\Delta T = 0$$

**END**