

FIDUCIAL MARKS AS MEASURES OF THIN FILM CRACK ARREST TOUGHNESS

Alex A. Volinsky¹, Michael L. Kottke¹, Neville R. Moody³, Indira S. Adhietty¹ and
William W. Gerberich²

¹ Motorola, Digital DNA™ Labs, Process and Materials Characterization Lab, Mesa, AZ.

² University of Minnesota, Dept. of Chem. Eng. and Mat. Science, Minneapolis, MN.

³ Sandia National Labs, Livermore, CA

ABSTRACT

Carbon fiducial marks are formed during thin film local delamination processes induced either by indentation, forming circular blisters, or by residual stress relief through telephone cord blister formations. Hydrocarbons are sucked into the crack tip during the delamination processes, outlining the crack tip opening angle (CTOA), which can be used to back calculate thin film adhesion using elastic or plastic analyses presented in the paper.

KEYWORDS

Fiducial marks, adhesion, fracture, delamination, crack arrest, crack tip opening angle, thin films

INTRODUCTION

Thin film adhesion can be measured by means of the superlayer indentation test [1-4]. Most good-adhered thin films can not be delaminated by means of regular indentation: films would rather deform plastically around the indenter by forming pileup. To prevent these problems a high modulus hard superlayer, capable of supporting and storing large amounts of elastic energy is deposited on top of the film of interest. Upon indentation a delamination blister forms around the indent, and its area is used to calculate the strain energy release rate (practical work of adhesion). This technique was shown to work with ductile metallic films (Al, Cu, Au, Cr) [2, 4-9, 15], ceramic (Ta₂N) [10, 12] and polymer films [16].

During indentation experiments into Cu thin films with a W superlayer it was found that the crack arrest marks form and correspond exactly to the blister size [13, 14]. Marks are formed of carbon, and outline the crack tip, representing its geometry [13, 14].

CRACK ARREST (FIDUCIAL) MARKS

Crack arrest marks were found after the blister removal with an adhesive tape. Scanning electron microscopy showed circles that correspond to the original blister diameter, and those were denoted as crack arrest fiducial marks [13, 14]. Atomic force microscopy was performed to measure the feature geometry, giving a width over 1 μm , and a height ranging from 5 to 15 nm. Contact and deflection AFM images of the partially removed blister showing the fiducial crack arrest marks are presented in Figure 1.

It was originally believed that the crack arrest mark is formed by crushed W and/or SiO_2 debris during the indentation [13]. More likely, however, radial cracking allowed laboratory air with moisture, hydrocarbons and surface debris to be sucked into the blister [14]. The exact source of contamination would be identified later, but whatever the source is, relatively mobile moisture, hydrocarbons and small debris particles were sucked into the crack tip leaving the fiducial mark detected in Figure 1.

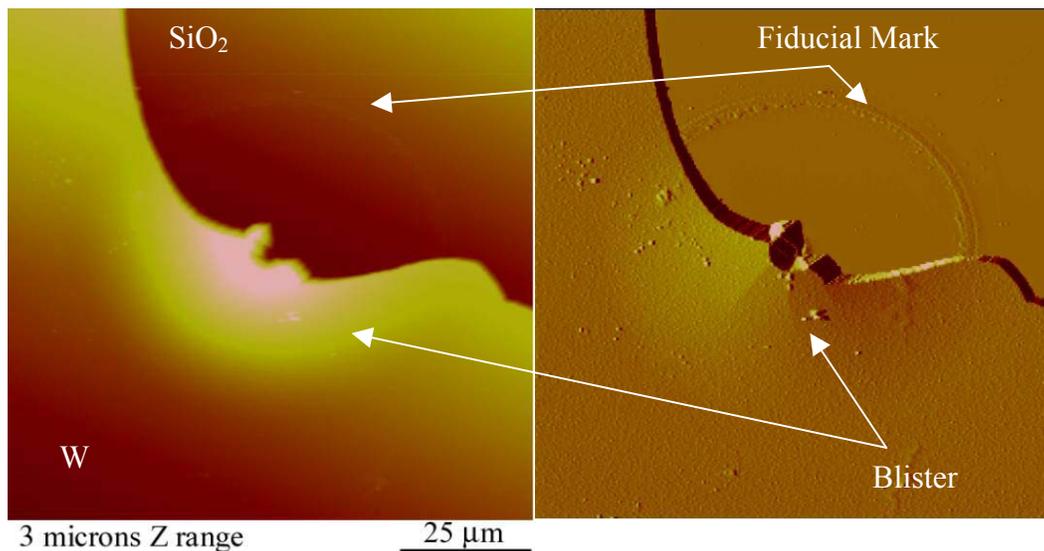


Figure 1. AFM height and deflection images of partially removed blister, showing fiducial mark underneath.

SLOW CRACK GROWTH ANALYSIS

Upon blister removal with a scotch tape the crack tip residue splits into two fiducial marks, leaving one on the film and substrate sides as shown in Figure 2. The substrate fiducial mark outlines the crack tip geometry, and its dimensions can be used to extract the thin film crack arrest toughness [13, 14].

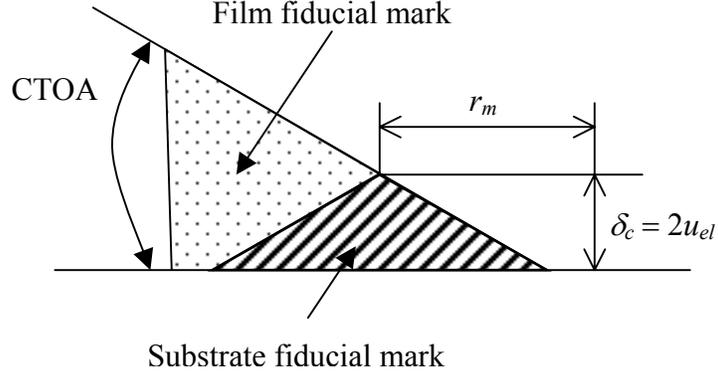


Figure 2. Fiducial mark geometry.

As discussed in [2, 4 and 15], brittle fracture is observed for thinner Cu films (< 100 nm) on Si substrates without a Ti underlayer. The majority of blisters in these films are buckled, so the crack is mostly under Mode I loading. This allows us to use the elastic crack tip opening displacement expressed for the plane stress tensile loading [17]:

$$u_{el}(r) = \frac{K}{E} \sqrt{\frac{8r}{\pi}} \quad (1).$$

AFM measurements of the fiducial mark on the substrate side provide the height, $\delta_c = 2u_{el}(r_m)$, and the half width of the mark, r_m (Figure 2), so K_I can be expressed as

$$K_I = \delta_c E \sqrt{\frac{\pi}{32r_m}} \quad (2).$$

From equation (2), for $\delta_c = 8$ nm and $r_m = 1$ μm one finds $K_I = 0.3$ $\text{MPa}\cdot\text{m}^{1/2}$. This is close to the 0.33 $\text{MPa}\cdot\text{m}^{1/2}$ value calculated from the actual G measurements (~ 0.9 J/m^2) for thinner Cu films using $K=(GE)^{1/2}$ for plane stress [2, 4, and 15]. Since the analysis is purely elastic, it indirectly proves that there is not much plastic energy dissipation at the crack tip for thin Cu films. Previously we also employed a plasticity-based slow crack growth approach based on the Rice, Drugan and Sham (RDS) analysis of the tearing modulus, T_0 [18] to show a similar result [13]. One can obtain a simple expression for strain energy release rate in terms of the crack-tip opening angle (CTOA in Figure 2):

$$J_{SS} = J_0 \exp\left(\frac{\alpha T_0}{\beta}\right) = J_0 \exp\left(\frac{E \cdot CTOA}{\sigma_{ys} \beta}\right) \quad (3),$$

where J_0 is the initial value of the J integral at crack initiation, T_0 is the tearing modulus, $\alpha \approx 1$, $\beta = 5.1$ from the mechanics description, E and σ_{ys} are modulus and yield strength. With 0.01 radians average value of the CTOA, a modulus of 120 GPa, a yield strength of 1 GPa and $\beta = 5.1$, one finds:

$$J_{SS} = J_0 \exp\{0.23\} \approx 1.27 J_0 \quad (4),$$

which means that during slow crack growth the strain energy release rate has barely increased for this 120 nm thick copper film. This again agrees with the actual measured value of $\sim 0.9 \text{ J/m}^2$ for the strain energy release rate.

CARBON CONTAMINATION SOURCE

There are three possible sources for carbon: adhesive tape, the diamond indenter and hydrocarbons from the atmosphere. In our previous studies the first two sources were eliminated [13-15], and hydrocarbons from the atmosphere were proposed as a source of fiducial mark formation.

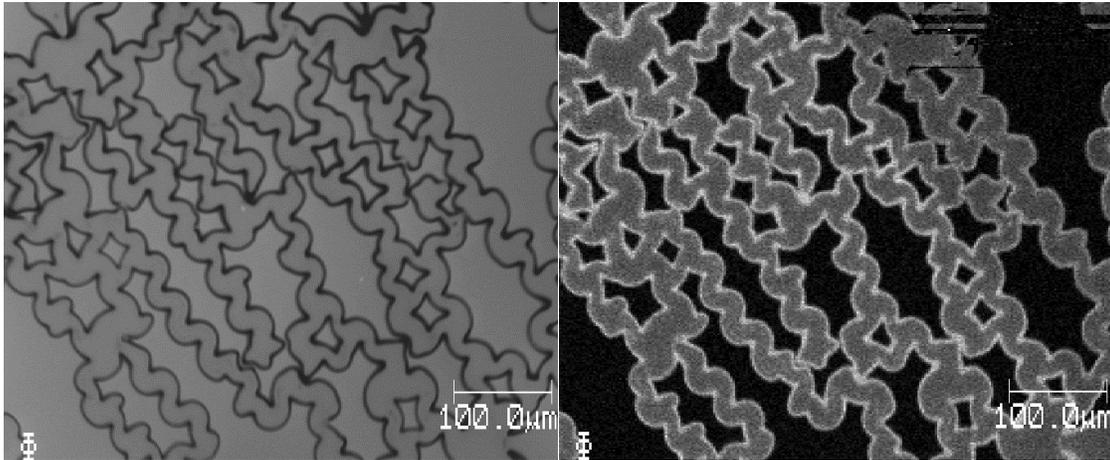


Figure 3. SEM micrograph and corresponding Carbon Auger map of a GaAs fracture surface upon TiW_xN_y film removal.

During the course of this study it was found that a similar type of contamination is present in a different film system of $\text{Ti}_x\text{W}_y\text{N}_z$ on GaAs, where the telephone cord delaminations formed due to the high residual stress relief (Figure 3). The carbon traces noted both on the film and substrate surfaces mimic the original telephone cord delamination pattern. Fiducial crack arrest marks are like those observed in the Cu/SiO₂ system. Figure 3 also shows a carbon Auger map, where brighter areas correspond to

higher carbon concentrations. There is almost no carbon present between the original phone cord delaminated areas (black regions in Figure 3). Most of the carbon goes into the crack tip, outlining the telephone cord topography. Fiducial mark formation may also be associated with the local heating at the crack tip. The heat dissipates fast enough so that the whole sample is not heated up, although the local crack tip temperature may increase substantially. This is a very interesting phenomenon that requires further investigation

ACKNOWLEDGEMENTS

The authors would like to acknowledge support through DOE grants DE-FG02/96ER45574 and DE-AC04-94AL85000. We would also like to acknowledge W. Miles Clift and Bernice E. Mills from Sandia National Lab at Livermore for Auger analysis and Robert F. Cook from the University of Minnesota for valuable discussions.

REFERENCES

1. Kriese M.D. and Gerberich W.W., (1999) *J. Mater. Res.* 14 (7), pp. 3007-18
2. Volinsky A.A., Tymiak N.I., Kriese M.D., Gerberich W.W. and Hutchinson J.W., (1999) *Mat. Res. Soc. Symp. Proc.* Vol. 539, pp. 277-290
3. Gerberich W.W., Kramer D.E., Tymiak N.I., Volinsky A.A., Bahr D.F., and Kriese M., (1999) *Acta mater.*, Vol. 47, No. 15, pp. 4115-4123
4. Tymiak N.I., Volinsky A.A., Kriese M.D., Downs S.A. and Gerberich W.W., (2000) *Metallurgical and Materials Transactions A*, Vol. 31A, pp. 863-872
5. Volinsky A.A., Moody N.R., Gerberich W.W., (2000) *MRS Symp. Proc.* Vol. 594
6. Moody N.R., Adams D., Volinsky A.A., Kriese M., Gerberich W.W., (2000) *Mat. Res. Soc. Symp. Proc.* Vol. 586
7. Schneider J.A., Guthrie S.E., Kriese M.D., Clift W.M., Moody N.R., (1999) *Materials Science & Engineering A (Structural Materials: Properties, Microstructure and Processing)*, Vol.A259, No.2 pp.253-60
8. Kriese M.D., Gerberich W.W., Moody N.R., (1999) *J. Mater. Res.* 14 (7), pp. 3019-26
9. Schneider J.A., Guthrie, S.E.; Kriese, M.D.; Clift, W.M.; Moody, N.R. (1998) *Fundamentals of Nanindentation and Nanotribology. Symposium* p.347-52
10. Moody N.R., Medlin D., Boehme D., Norwood D.P., (1998) *Engineering Fracture Mechanics*, Vol.61, no.1 p.p107-18
11. Moody, N.R.; Hwang, R.Q.; Venka-Taramani, S.; Angelo, J.E.; Norwood, D.P.; Gerberich, W.W. (1998), *Acta Materialia* vol.46, no.2 p.585-97
12. Moody, N.R.; Medlin, D.; Norwood, D.P.; Gerberich, W.W.; Gao, H.; Sundgren, J.-E.; Baker, S.P. (1997) *Thin Films: Stresses and Mechanical Properties VI. Symposium* p.97-102
13. Volinsky A.A., Gerberich W.W., (1999) *MRS Symp. Proc.* Vol. 563, p.275-84
14. Volinsky A.A., Clift W.M., Moody N.R., Gerberich W.W., (1999) *Mat. Res. Soc. Symp. Proc.* Vol. 586
15. Volinsky A.A., (2000) Ph.D. Dissertation, University of Minnesota

16. Volinsky A.A., Vella J.B., Fowler B.W., Adhietty I.S., Gerberich W.W., (2001)
presented at 2001 Mechanics and Materials Summer Conference, San Diego
17. Lawn B., (1993) "Fracture of Brittle Solids", Cambridge University Press,
Cambridge
18. Anderson T.L., (1991) "Fracture Mechanics: Fundamentals and Applications." CRC
Press, Boston, p. 219